

NCV890131

1.2 A, 2 MHz Automotive Buck Switching Regulator

The NCV890131 is a fixed-frequency, monolithic, Buck switching regulator intended for Automotive, battery-connected applications that must operate with up to a 36 V input supply. The regulator is suitable for systems with low noise and small form factor requirements often encountered in automotive driver information systems. The NCV890131 is capable of converting the typical 4.5 V to 18 V automotive input voltage range to outputs as low as 3.3 V at a constant switching frequency above the sensitive AM band, eliminating the need for costly filters and EMI countermeasures. Two pins are provided to synchronize switching to a clock, or to another NCV890131. The NCV890131 also provides several protection features expected in Automotive power supply systems such as current limit, short circuit protection, and thermal shutdown. In addition, the high switching frequency produces low output voltage ripple even when using small inductor values and an all-ceramic output filter capacitor – forming a space-efficient switching regulator solution.

Features

- Internal N-Channel Power Switch
- Low V_{IN} Operation Down to 4.5 V
- High V_{IN} Operation to 36 V
- Withstands Load Dump to 45 V
- 2 MHz Free-running Switching Frequency
- Auto-synchronizes with Other NCV890131 or to an External Clock
- Logic level Enable Input Can be Directly Tied to Battery
- 1.4 A (min) Cycle-by-Cycle Peak Current Limit
- Short Circuit Protection enhanced by Frequency Foldback
- $\pm 1.75\%$ Output Voltage Tolerance
- Output Voltage Adjustable Down to 0.8 V
- 1.4 Millisecond Internal Soft-Start
- Thermal Shutdown (TSD)

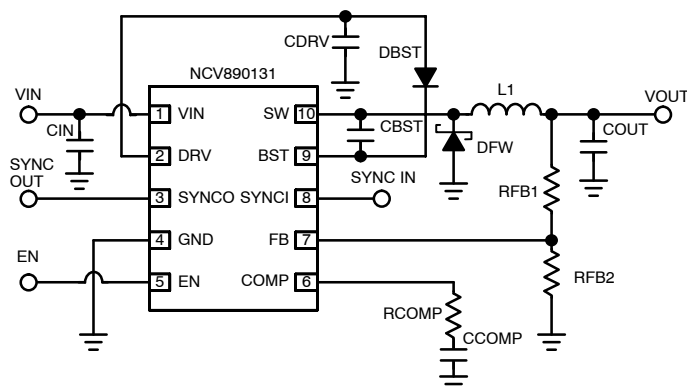


Figure 1. Typical Application



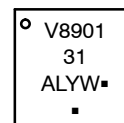
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MARKING DIAGRAM



DFN10
CASE 485C



- A = Assembly Location
- L = Wafer Lot
- Y = Year
- W = Work Week
- = Pb-Free Device

(*Note: Microdot may be in either location)

ORDERING INFORMATION

See detailed ordering and shipping information in the package dimensions section on page 14 of this data sheet.

- Low Shutdown Current
- Wettable Flanks – DFN
- NCV Prefix for Automotive and Other Applications Requiring Unique Site and Control Change Requirements; AEC-Q100 Qualified and PPAP Capable
- These Devices are Pb-Free and are RoHS Compliant

Applications

- Audio
- Infotainment
- Safety – Vision Systems
- Instrumentation

NCV890131

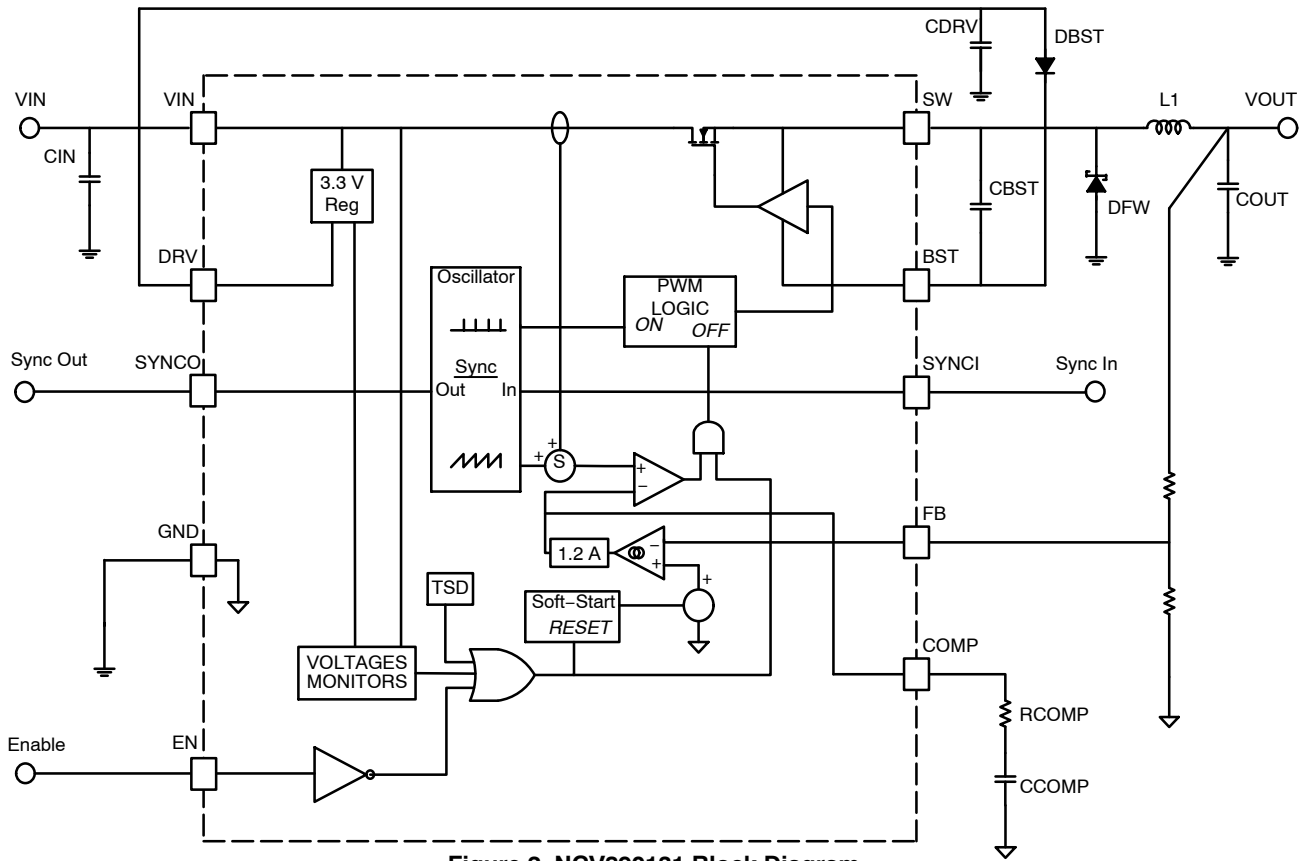


Figure 2. NCV890131 Block Diagram

MAXIMUM RATINGS

Rating	Symbol	Value	Unit
Min/Max Voltage VIN		-0.3 to 45	V
Max Voltage VIN to SW		45	V
Min/Max Voltage SW		-0.7 to 40	V
Min Voltage SW – 20ns		-3.0	V
Min/Max Voltage BST		-0.3 to 40	
Min/Max Voltage BST to SW		-0.3 to 3.6	V
Min/Max Voltage on EN		-0.3 to 40	V
Min/Max Voltage COMP		-0.3 to 2	V
Min/Max Voltage FB		-0.3 to 18	V
Min/Max Voltage SYNCO		-0.3 to 3.6	V
Min/Max Voltage DRV		-0.3 to 3.6	V
Min/Max Voltage SYNCI		-0.3 to 6	V
Thermal Resistance, 3x3 DFN Junction-to-Ambient*	R _{θJA}	50	°C/W
Storage Temperature range		-55 to +150	°C
Operating Junction Temperature Range	T _J	-40 to +150	°C
ESD withstand Voltage	Human Body Model Machine Model Charge Device Model	2.0 200 >1.0	kV V kV
Moisture Sensitivity	MSL	Level 1	
Peak Reflow Soldering Temperature		260	°C

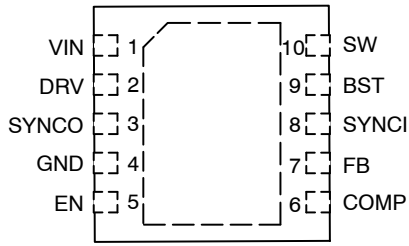
Stresses exceeding Maximum Ratings may damage the device. Maximum Ratings are stress ratings only. Functional operation above the Recommended Operating Conditions is not implied. Extended exposure to stresses above the Recommended Operating Conditions may affect device reliability.

*Mounted on 1 sq. in. of a 4-layer PCB with 1 oz. copper thickness.

RECOMMENDED OPERATING CONDITIONS:

Rating	Value	Unit
V _{IN} Range	4.5 to 36	V
Ambient Temperature Range	-40 to 105	°C

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(Top View)

Figure 3. Pin Connections

PIN FUNCTION DESCRIPTIONS

Pin No.	Symbol	Description
1	VIN	Input voltage from battery. Place an input filter capacitor in close proximity to this pin.
2	DRV	Output voltage to provide a regulated voltage to the Power Switch gate driver.
3	SYNCO	Synchronization output. Turn-on of the Power Switch causes the SYNCO signal to fall. SYNCO rises half a switching period later. Connecting to the SYNCI pin of another NCV890131 causes them to switch out-of-phase
4	GND	Battery return, and output voltage ground reference.
5	EN	This TTL compatible Enable input allows the direct connection of Battery as the enable signal. Grounding this input stops switching and reduces quiescent current draw to a minimum.
6	COMP	Error Amplifier output, for tailoring transient response with external compensation components.
7	FB	Feedback input pin to program output voltage, and detect pre-charged or shorted output conditions.
8	SYNCI	Synchronization input. Connecting an external clock to the SYNCI pin synchronizes switching to the rising edge of the SYNCI voltage.
9	BST	Bootstrap input provides drive voltage higher than VIN to the N-channel Power Switch for optimum switch $R_{DS(on)}$ and highest efficiency.
10	SW	Switching node of the Regulator. Connect the output inductor and cathode of the freewheeling diode to this pin.
Exposed Pad		Connect to Pin 4 (electrical ground) and to a low thermal resistance path to the ambient temperature environment.

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ELECTRICAL CHARACTERISTICS ($V_{IN} = 4.5\text{ V to }28\text{ V}$, $V_{EN} = 5\text{ V}$, $V_{BST} = V_{SW} + 3.0\text{ V}$, $C_{DRV} = 0.1\text{ }\mu\text{F}$, Min/Max values are valid for the temperature range $-40^{\circ}\text{C} \leq T_J \leq 150^{\circ}\text{C}$ unless noted otherwise, and are guaranteed by test, design or statistical correlation.)

Parameter	Symbol	Conditions	Min	Typ	Max	Unit
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QUIESCENT CURRENT

Quiescent Current, shutdown	I_{qSD}	$V_{IN} = 13.2\text{ V}$, $V_{EN} = 0\text{ V}$, $T_J = 25^{\circ}\text{C}$			10	μA
Quiescent Current, enabled	I_{qEN}	$V_{IN} = 13.2\text{ V}$			3.0	mA

UNDERVOLTAGE LOCKOUT - VIN (UVLO)

UVLO Start Threshold	V_{UVLSTT}	V_{IN} rising	4.1		4.5	V
UVLO Stop Threshold	V_{UVLSTP}	V_{IN} falling	3.9		4.4	V
UVLO Hysteresis	V_{UVLOHY}		0.1		0.2	V

ENABLE (EN)

Logic Low	V_{ENLO}		0.8			V
Logic High	V_{ENHI}				2.0	V
Input Current	I_{EN}		8.0		30	μA

SOFT-START (SS)

Soft-Start Completion Time	t_{SS}		0.8	1.4	2.0	ms
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VOLTAGE REFERENCE

FB Pin Voltage during regulation	V_{FBR}	COMP shorted to FB	0.786	0.8	0.814	V
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ERROR AMPLIFIER

FB Bias Current	I_{FBBIAS}	$V_{FB} = 0.8\text{ V}$	0.25		1.0	μA
Transconductance	g_m $g_{m(HV)}$	$V_{COMP} = 1.3\text{ V}$ $4.5\text{ V} < V_{IN} < 18\text{ V}$ $20\text{ V} < V_{IN} < 28\text{ V}$	0.6 0.3	1.0 0.5	1.5 0.75	mmho
Output Resistance	R_{OUT}			1.4		$\text{M}\Omega$
COMP Source Current Limit	I_{SOURCE}	$V_{FB} = 0.63\text{ V}$, $V_{COMP} = 1.3\text{ V}$ $4.5\text{ V} < V_{IN} < 18\text{ V}$ $20\text{ V} < V_{IN} < 28\text{ V}$		75 40		μA
COMP Sink Current Limit	I_{SINK}	$V_{FB} = 0.97\text{ V}$, $V_{COMP} = 1.3\text{ V}$ $4.5\text{ V} < V_{IN} < 18\text{ V}$ $20\text{ V} < V_{IN} < 28\text{ V}$		75 40		μA
Minimum COMP voltage	V_{CMPMIN}	$V_{FB} = 0.97\text{ V}$	0.2		0.7	V

OSCILLATOR

Frequency	F_{SW} $F_{SW(HV)}$	$4.5 < V_{IN} < 18\text{ V}$ $20\text{ V} < V_{IN} < 28\text{ V}$	1.8 0.9	2.0 1.0	2.2 1.1	MHz
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VIN FREQUENCY FOLDBACK MONITOR

Frequency Foldback Threshold V_{IN} rising V_{IN} falling	V_{FLDUP} V_{FLDDN}	$V_{FB} = 0.63\text{ V}$	18.4 18		20 19.8	V
Frequency Foldback Hysteresis	V_{FLDHY}		0.2	0.3	0.4	V

SYNCHRONIZATION

SYNCO Output Pulse Duty Ratio	$D_{(SYNC)}$	$C_{LOAD} = 40\text{ pF}$	40		60	%
SYNCO Output Pulse Falltime	$t_{R(SYNC)}$	$C_{LOAD} = 40\text{ pF}$, 90% to 10%		4		ns
SYNCO Output Pulse Risettime	$t_{F(SYNC)}$	$C_{LOAD} = 40\text{ pF}$, 10% to 90%		4		ns
SYNCI Input Resistance to ground	$R_{H(SYNC)}$	$V_{SYNCI} = 5.0\text{ V}$	50		200	$\text{k}\Omega$
SYNCI Input High Threshold Voltage	V_{HSYNC}				2.0	V
SYNCI Input Low Threshold Voltage	V_{LSYNC}		0.8			V
SYNCI High Pulse Width	t_{HSYNCI}	$V_{SYNCO} > \max V_{HSYNCI}$	40			ns

1. Not tested in production. Limits are guaranteed by design.

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Parameter	Symbol	Conditions	Min	Typ	Max	Unit
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SYNCHRONIZATION

SYNCl Low Pulse Width	t_{LSYNCl}	$V_{SYNCl} < \min V_{LSYNCl}$	40			ns
External Sync Frequency	F_{SYNCl}		1.8		2.5	MHz
Master Reassertion Time	$t_{I(SYNCl)}$	Time from last rising SYNCl edge to first un-synchronized turn-on.		650		ns

VIN OVERVOLTAGE SHUTDOWN MONITOR

Overvoltage Stop Threshold	V_{OVSTP}		32.4		36	V
Overvoltage Start Threshold	V_{OVSTT}		30		35.4	V
Overvoltage Hysteresis	V_{OVHY}		0.6	1.5	2.4	V

SLOPE COMPENSATION

Ramp Slope (Note 1) (With respect to switch current)	S_{ramp} $S_{ramp(HV)}$	$4.5 < V_{IN} < 18\text{ V}$ $20\text{ V} < V_{IN} < 28\text{ V}$	0.7 0.25		1.3 0.6	A/ μs
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POWER SWITCH

ON Resistance	R_{DSON}	$V_{BST} = V_{SW} + 3.0\text{ V}$			650	m Ω
Leakage current VIN to SW	I_{LKSW}	$V_{EN} = 0\text{ V}$, $V_{SW} = 0$, $V_{IN} = 18\text{ V}$			10	μA
Minimum ON Time	t_{ONMIN}	Measured at SW pin	45		70	ns
Minimum OFF Time	t_{OFFMIN}	Measured at SW pin At $F_{SW} = 2\text{ MHz}$ (normal) At $F_{SW} = 500\text{ kHz}$ (max duty cycle)	30	30 50	70	ns

PEAK CURRENT LIMIT

Current Limit Threshold	I_{LIM}		1.4	1.55	1.7	A
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SHORT CIRCUIT FREQUENCY FOLDBACK

Lowest Foldback Frequency	F_{SWAF}	$V_{FB} = 0\text{ V}$, $4.5\text{ V} < V_{IN} < 18\text{ V}$	400	500	600	kHz
Lowest Foldback Frequency – High V_{in}	F_{SWAFHV}	$V_{FB} = 0\text{ V}$, $20\text{ V} < V_{IN} < 28\text{ V}$	200	250	300	
Hiccup Mode	F_{SWHIC}	$V_{FB} = 0\text{ V}$	24	32	40	

GATE VOLTAGE SUPPLY (DRV pin)

Output Voltage	V_{DRV}		3.1	3.3	3.5	V
DRV POR Start Threshold	V_{DRVSTT}		2.7	2.9	3.05	V
DRV POR Stop Threshold	V_{DRVSTP}		2.5	2.8	3.0	V
DRV Current Limit	I_{DRVLM}	$V_{DRV} = 0\text{ V}$	16		45	mA

OUTPUT PRECHARGE DETECTOR

Threshold Voltage	V_{SSEN}		20	35	50	mV
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THERMAL SHUTDOWN

Activation Temperature (Note 1)	T_{SD}		150		190	$^{\circ}\text{C}$
Hysteresis (Note 1)	T_{HYS}		5		20	$^{\circ}\text{C}$

1. Not tested in production. Limits are guaranteed by design.

TYPICAL CHARACTERISTICS CURVES

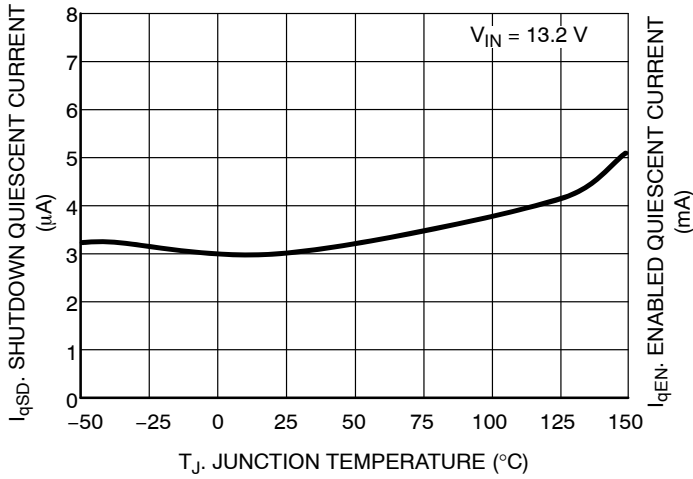


Figure 4. Shutdown Quiescent Current vs. Junction Temperature

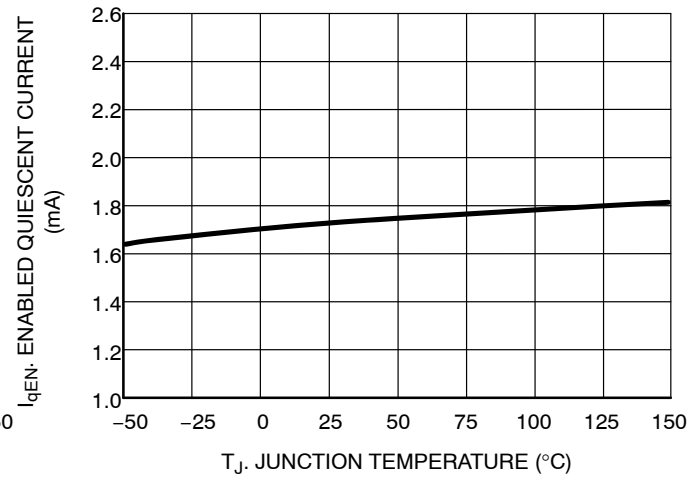


Figure 5. Enabled Quiescent Current vs. Junction Temperature

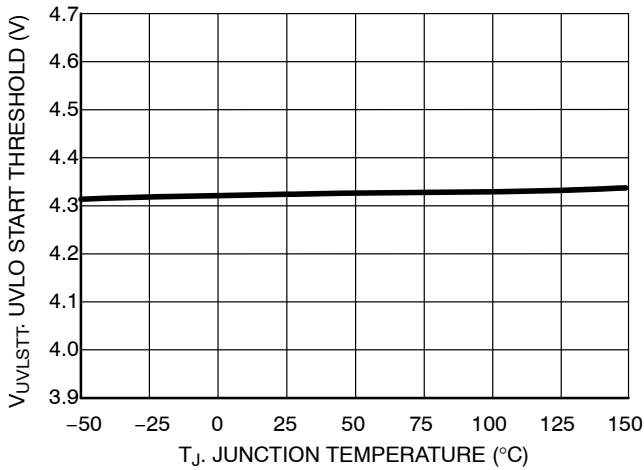


Figure 6. UVLO Start Threshold vs. Junction Temperature

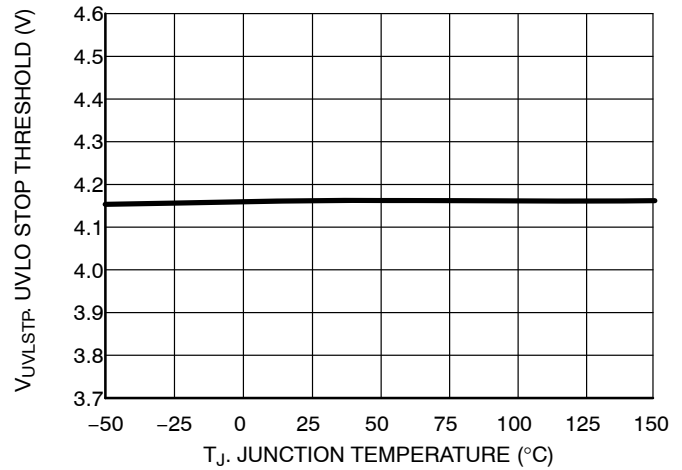


Figure 7. UVLO Stop Threshold vs. Junction Temperature

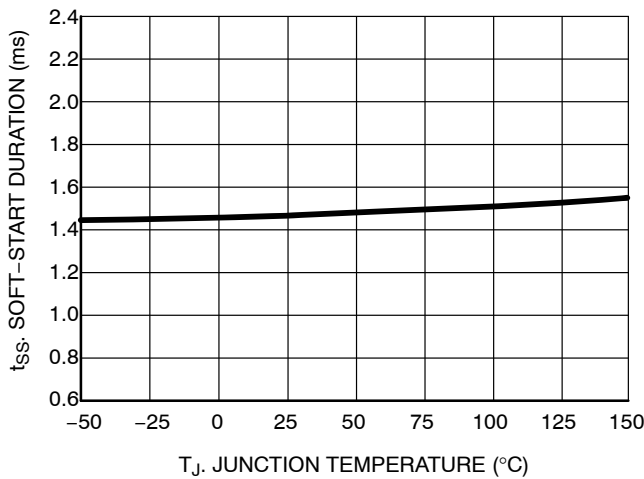


Figure 8. Soft-Start Duration vs. Junction Temperature

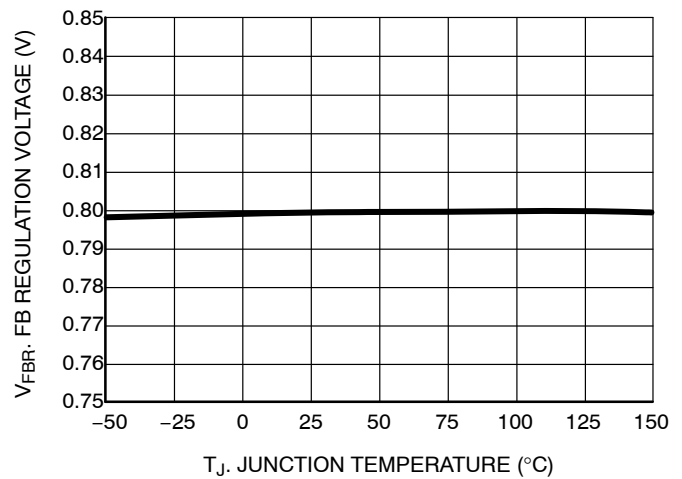


Figure 9. FB Regulation Voltage vs. Junction Temperature

TYPICAL CHARACTERISTICS CURVES

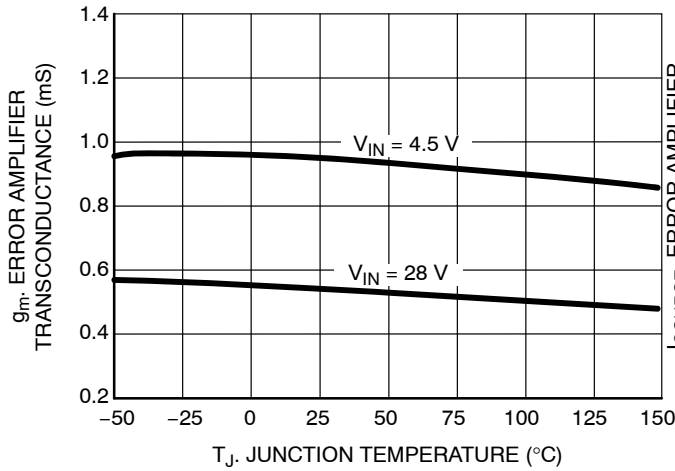


Figure 10. Error Amplifier Transconductance vs. Junction Temperature

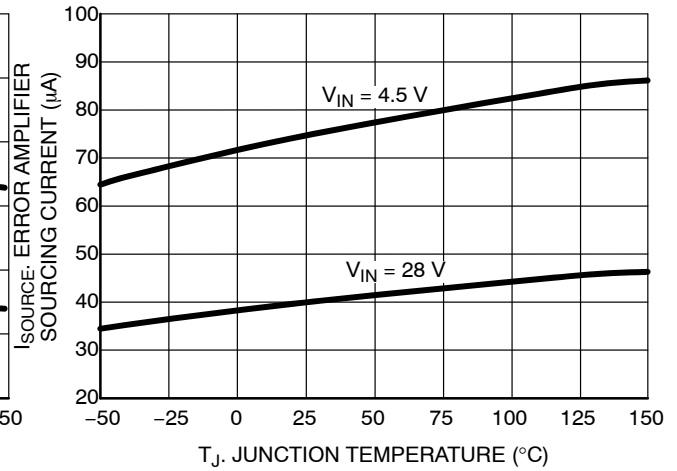


Figure 11. Error Amplifier Max Sourcing Current vs. Junction Temperature

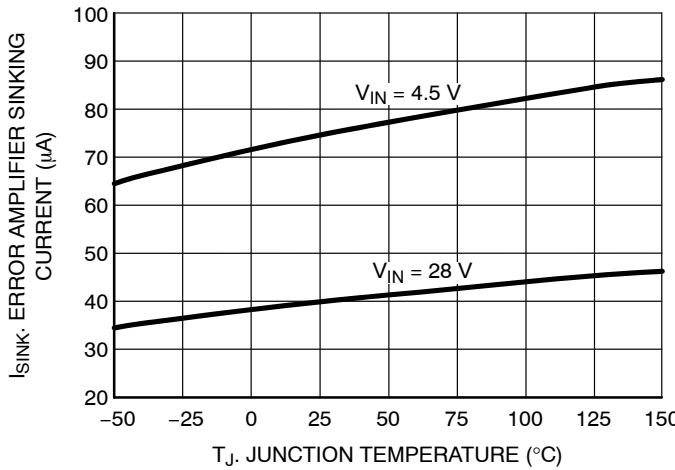


Figure 12. Error Amplifier Max Sinking Current vs. Junction Temperature

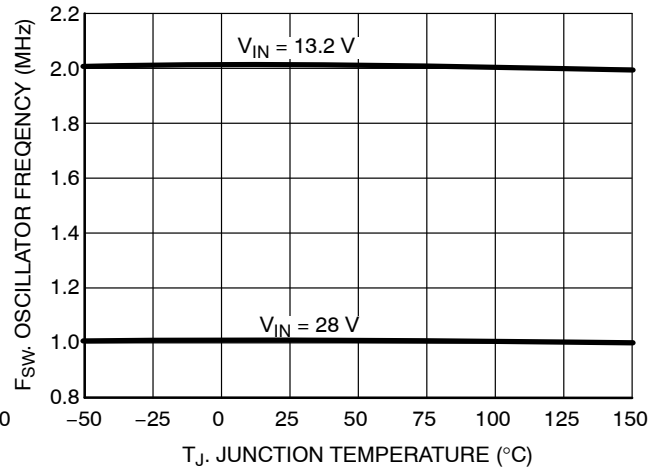


Figure 13. Oscillator Frequency vs. Junction Temperature

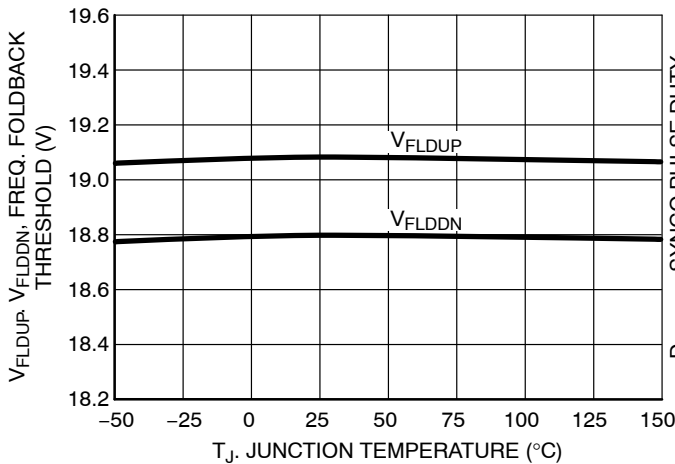


Figure 14. Rising Frequency Foldback Threshold vs. Junction Temperature

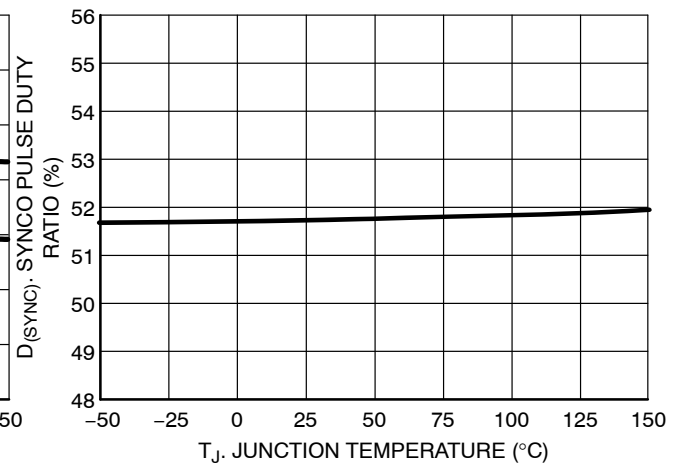


Figure 15. SYNCO Pulse Duty Ratio vs. Junction Temperature

TYPICAL CHARACTERISTICS CURVES

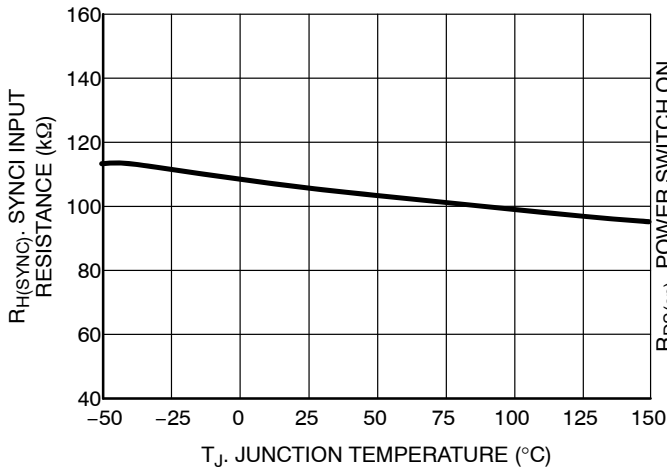


Figure 16. SYNCl Input Resistance vs. Junction Temperature

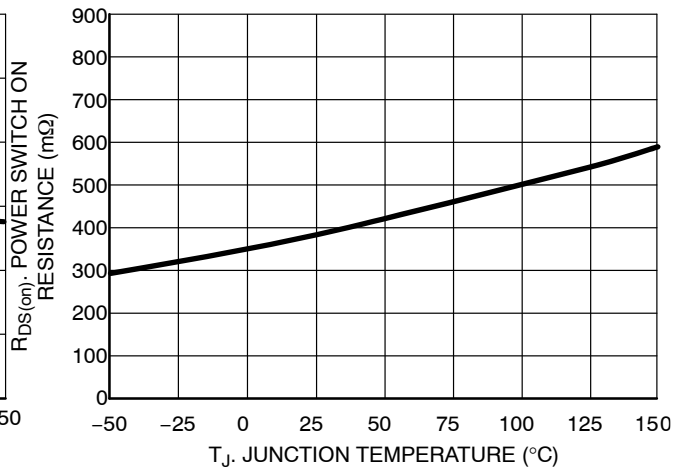


Figure 17. Power Switch R_{DS(on)} vs. Junction Temperature

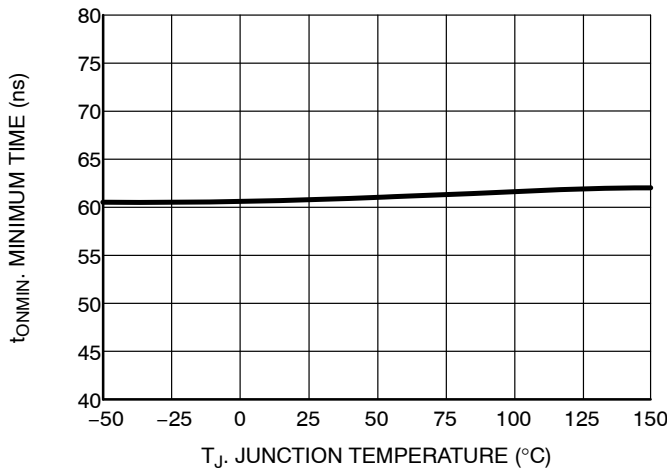


Figure 18. Minimum On Time vs. Junction Temperature

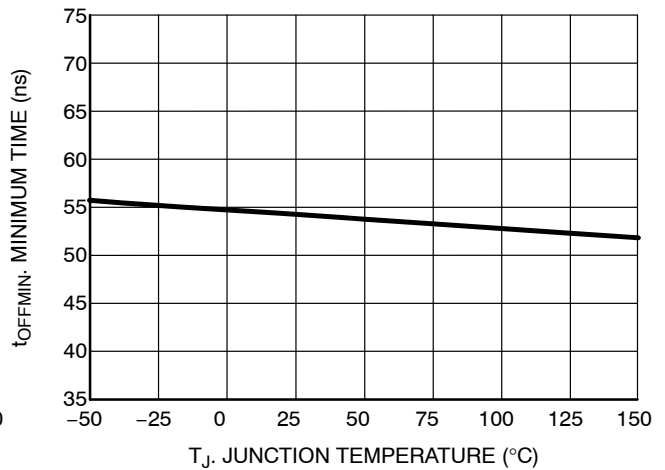


Figure 19. Minimum Off Time vs. Junction Temperature

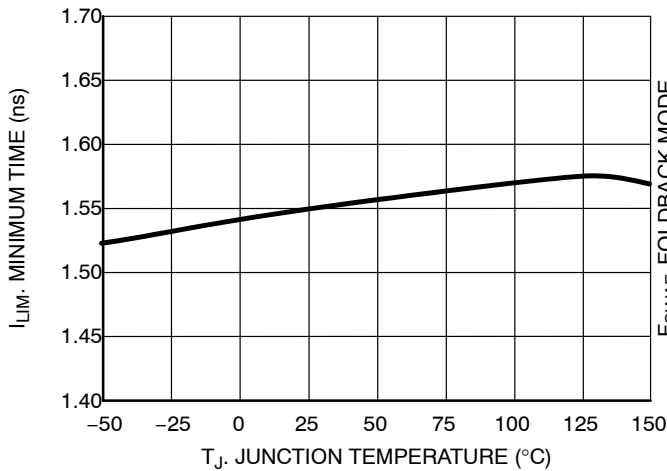


Figure 20. Current Limit Threshold vs. Junction Temperature

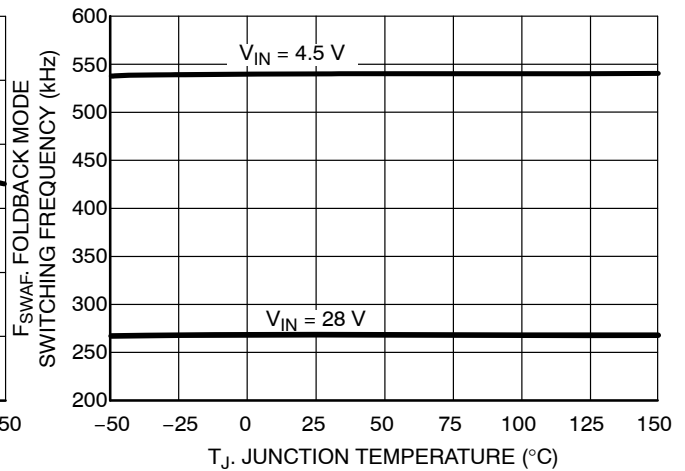


Figure 21. Short-Circuit Foldback Frequency vs. Junction Temperature

TYPICAL CHARACTERISTICS CURVES

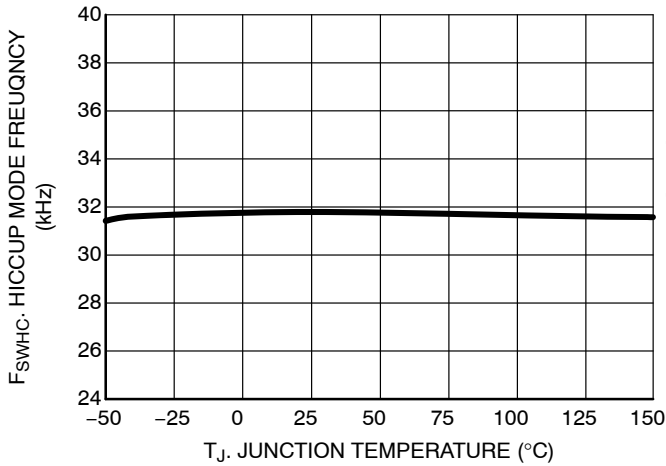


Figure 22. Hiccup Mode Switching Frequency vs. Junction Temperature

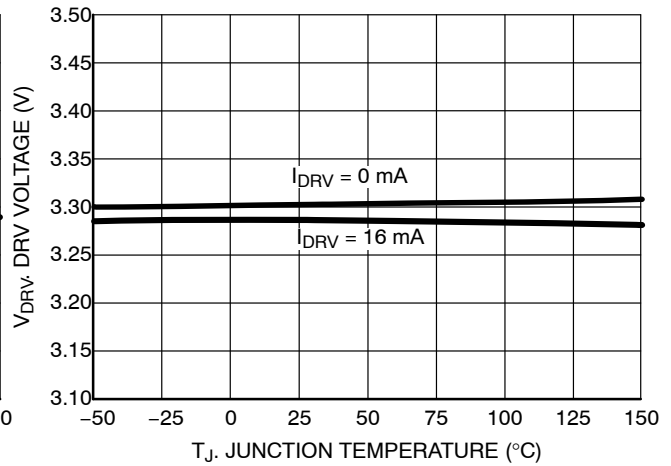


Figure 23. DRV Voltage vs. Junction Temperature

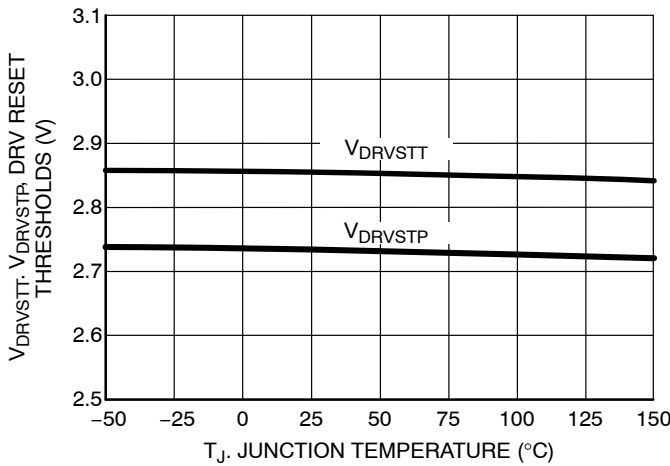


Figure 24. DRV Reset Threshold vs. Junction Temperature

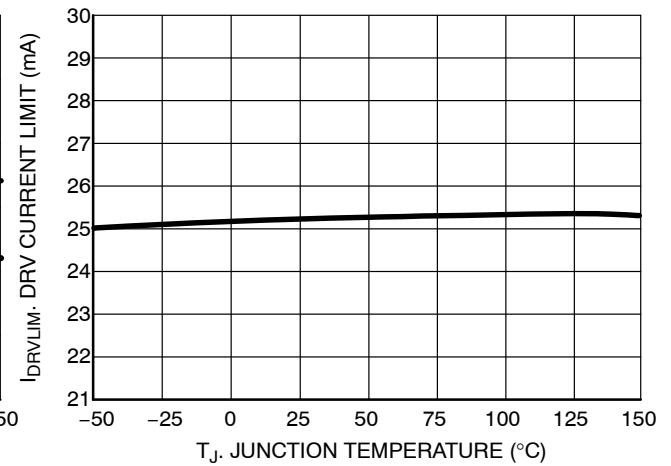


Figure 25. DRV Current Limit vs. Junction Temperature

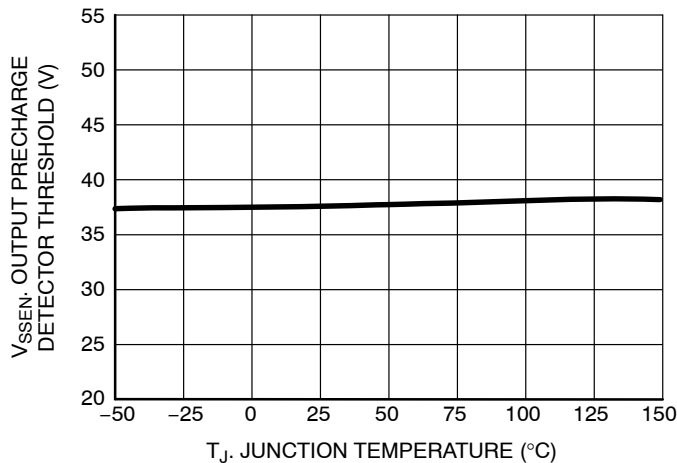


Figure 26. Output Precharge Detector Threshold vs. Junction Temperature

GENERAL INFORMATION

INPUT VOLTAGE

An Undervoltage Lockout (UVLO) circuit monitors the input, and inhibits switching and resets the Soft-start circuit if there is insufficient voltage for proper regulation. The NCV890131 can regulate a 3.3 V output with input voltages above 4.5 V and a 5.0 V output with an input above 6.5 V.

The NCV890131 automatically terminates switching if input voltage exceeds V_{OVSTP} (see Figure 27), and withstands input voltages up to 45 V.

To limit the power lost in generating the drive voltage for the Power Switch, the switching frequency is reduced by a factor of 2 when the input voltage exceeds the V_{IN} Frequency Foldback threshold V_{FLDUP} (see Figure 27). Frequency reduction is automatically terminated when the input voltage drops back below the V_{IN} Frequency Foldback threshold V_{FLDDN} .

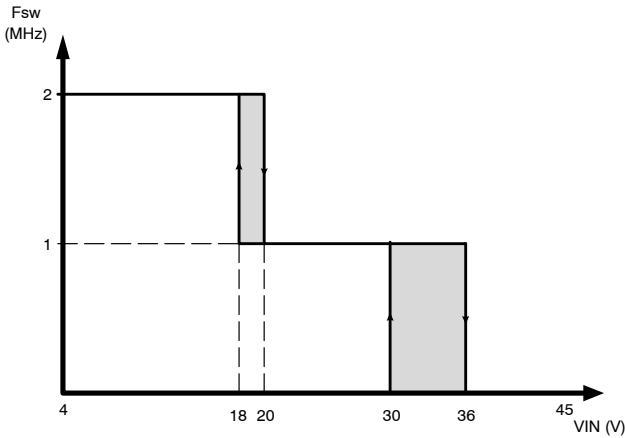


Figure 27. NCV890131 Switching Frequency Reduction at High Input Voltage

ENABLE

The NCV890131 is designed to accept either a logic level signal or battery voltage as an Enable signal. EN low induces a 'sleep mode' which shuts off the regulator and minimizes its supply current to a couple of μA typically (I_{qSD}) by disabling all functions. Upon enabling, voltage is established at the DRV pin, followed by a soft-start of the switching regulator output.

SOFT-START

Upon being enabled or released from a fault condition, and after the DRV voltage is established, a soft-start circuit ramps the switching regulator error amplifier reference voltage to the final value. During soft-start, the average switching frequency is lower than its normal mode value (typically 2 MHz) until the output voltage approaches regulation.

ERROR AMPLIFIER

The error amplifier is a transconductance type amplifier. The output voltage of the error amplifier controls the peak

inductor current at which the power switch shuts off. The Current Mode control method employed by the NCV890131 allows the use of a simple, Type II compensation to optimize the dynamic response according to system requirements.

SLOPE COMPENSATION

A fixed slope compensation signal is generated internally and added to the sensed current to avoid increased output voltage ripple due to bifurcation of inductor ripple current at duty cycles above 50%. The fixed amplitude of the slope compensation signal requires the inductor to be greater than a minimum value, depending on output voltage, in order to avoid sub-harmonic oscillations. For 3.3 V and 5 V output voltages, the recommended inductor value is 4.7 μH .

SHORT CIRCUIT FREQUENCY FOLDBACK

During severe output overloads or short circuits, the NCV890131 automatically reduces its switching frequency. This creates duty cycles small enough to limit the peak current in the power components, while maintaining the ability to automatically reestablish the output voltage if the overload is removed. If the current is still too high after the switching frequency folds back to 500 kHz, the regulator enters an auto-recovery burst mode that further reduces the dissipated power.

CURRENT LIMITING

Due to the ripple on the inductor current, the average output current of a buck converter is lower than the peak current setpoint of the regulator. Figure 28 shows – for a 4.7 μH inductor – how the variation of inductor peak current with input voltage affects the maximum DC current the NCV890131 can deliver to a load.

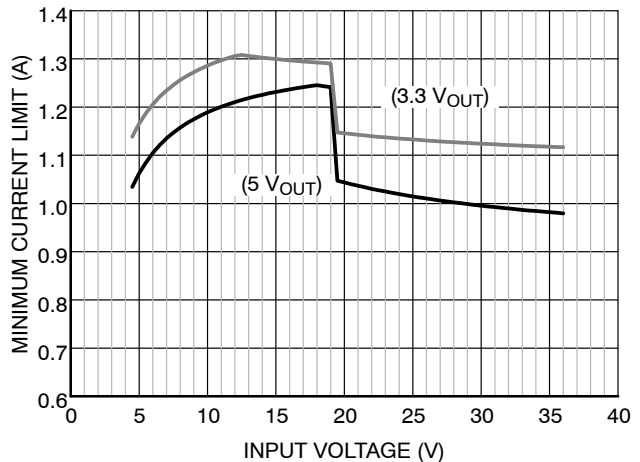


Figure 28. NCV890131 Load Current Capability with 4.7 μH Inductor

NCV890131

SYNCHRONIZATION

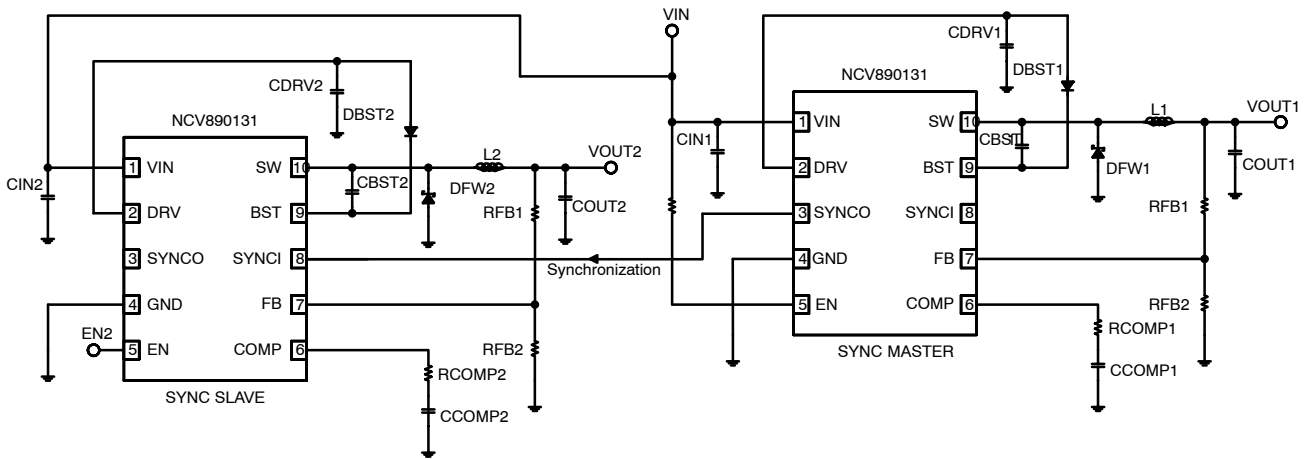
Two NCV890131 can be synchronized out-of-phase to one another by connecting the SYNCO pin of one to the SYNCI pin of the other (Figure 29). Any number of NCV890131 can also be synchronized to an external clock (Figure 30). If a part does not have its switching frequency controlled by the SYNCI input, it drives the SYNCO pin low when it turns on the power switch, and drives it high half a switching period later. When the switching frequency is controlled by the SYNCI input, the SYNCO pin is held low. Synchronization starts within 2 ms of soft-start completion.

A rising edge at the SYNCI pin causes an NCV890131 to immediately turn on the power switch. If another rising edge

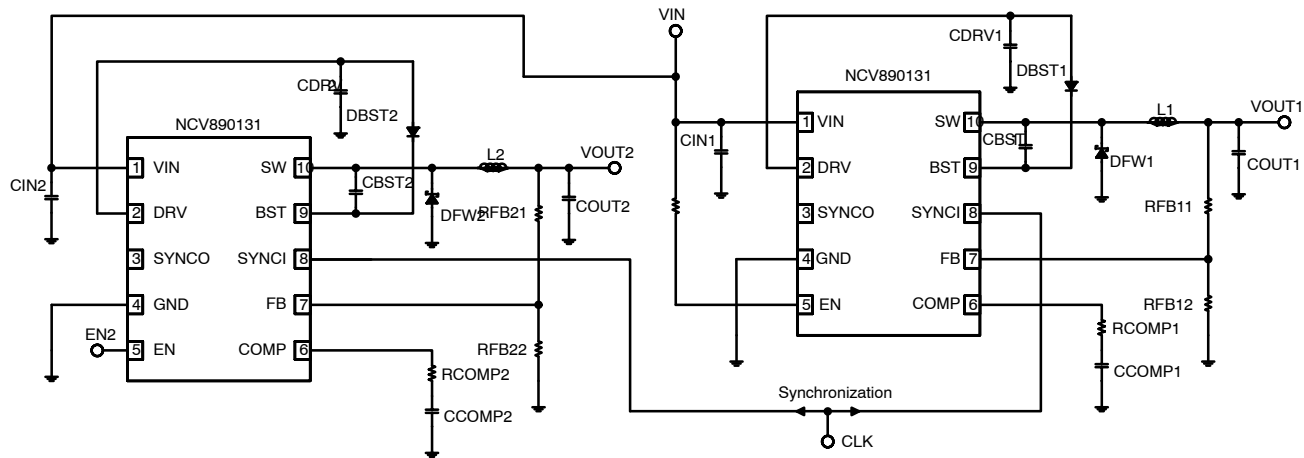
does not arrive at the SYNCI pin within the Master Reassertion Time, the NCV890131 controls its own switching frequency, allowing uninterrupted operation in the event that the clock (or controlling NCV890131) is turned off.

If internal conditions or excessive input voltage cause an NCV890131 to fold back its switching frequency, the main oscillator switching frequency is still derived from the frequency received at the SYNCI pin. Under these conditions, the SYNCO pin is held low.

An external pulldown resistor is not required at the SYNCI pin if it is unconnected.



**Figure 29. NCV890131s Synchronized to Each Other
Master Enabled by Battery**



**Figure 30. Both NCV890131s Synchronized to External Clock
#1 Enabled by Battery**

BOOTSTRAP

At the DRV pin an internal regulator provides a ground-referenced voltage to an external capacitor (C_{DRV}), to allow fast recharge of the external bootstrap capacitor (C_{BST}) used to supply power to the power switch gate driver. If the voltage at the DRV pin goes below the DRV UVLO Threshold V_{DRVSTB} switching is inhibited and the Soft-start circuit is reset, until the DRV pin voltage goes back up above V_{DRVSTT} .

In order for the bootstrap capacitor to stay charged, the Switch node needs to be pulled down to ground regularly. In very light load condition, the NCV890131 skips switching cycles to ensure the output voltage stays regulated. When the skip cycle repetition frequency gets too low, the bootstrap voltage collapses and the regulator stops switching. Practically, this means that the NCV890131 needs a minimum load to operate correctly: to cover all conditions of input voltage and temperature, this minimum load is 8 mA.

OUTPUT PRECHARGE DETECTION

Prior to Soft-start, the FB pin is monitored to ensure the SW voltage is low enough to have charged the external bootstrap capacitor (C_{BST}). If the FB pin is higher than V_{SSEN} , restart is delayed until the output has discharged.

THERMAL SHUTDOWN

A thermal shutdown circuit inhibits switching, resets the Soft-start circuit, and removes DRV voltage if internal temperature exceeds a safe level. Switching is automatically restored when temperature returns to a safe level.

MINIMUM DROPOUT VOLTAGE

When operating at low input voltages, two parameters play a major role in imposing a minimum voltage drop across the regulator: the minimum off time (that sets the maximum duty cycle), and the on state resistance.

When operating in continuous conduction mode (CCM), the output voltage is equal to the input voltage multiplied by the duty ratio. Because the NCV890131 needs a sufficient bootstrap voltage to operate, its duty cycle cannot be 100%: it needs a minimum off time (t_{OFFmin}) to periodically re-fuel the bootstrap capacitor C_{BST} . This imposes a maximum duty ratio $D_{MAX} = 1 - t_{OFFmin} \cdot F_{SW(min)}$, with the switching frequency being folded back down to $F_{SW(min)} = 500$ kHz to keep regulating at the lowest input voltage possible.

The drop due to the on-state resistance is simply the voltage drop across the Switch resistance R_{DSon} at the given output current: $V_{SWdrop} = I_{OUT} \cdot R_{DSon}$.

Which leads to the maximum output voltage in low V_{in} condition: $V_{OUT} = D_{MAX} \cdot V_{IN(min)} - V_{SWdrop}$

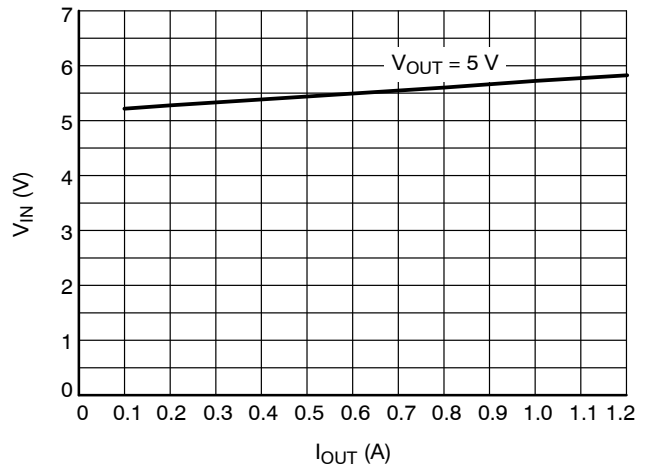


Figure 31. Minimum Input Voltage vs. Output Current

EXPOSED PAD

The exposed pad (EPAD) on the back of the package must be electrically connected to the electrical ground (GND pin) for proper, noise-free operation.

DESIGN METHODOLOGY

The NCV890131 being a fixed-frequency regulator with the switching element integrated, is optimized for one value of inductor. This value is set to 4.7 μ H, and the slope compensation is adjusted for this inductor. The only components left to be designed are the input and output capacitor and the freewheeling diode.

Output capacitor:

The minimum output capacitor value can be calculated based on the specification for output voltage ripple:

$$C_{OUTmin} = \frac{\Delta I_L}{8 \cdot \Delta V_{OUT} \cdot F_{SW}} \quad (\text{eq. 1})$$

With

- ΔI_L the inductor ripple current:

$$\Delta I_L = \frac{V_{OUT} \cdot \left(1 - \frac{V_{OUT}}{V_{IN}}\right)}{L \cdot F_{SW}} \quad (\text{eq. 2})$$

- ΔV_{OUT} the desired voltage ripple.

However, the ESR of the output capacitor also contributes to the output voltage ripple, so to comply with the requirement, the ESR cannot exceed R_{ESRmax} :

$$R_{ESRmax} = \frac{\Delta V_{OUT} \cdot L \cdot F_{SW}}{V_{OUT} \cdot \left(1 - \frac{V_{OUT}}{V_{IN}}\right)} \quad (\text{eq. 3})$$

Finally, the output capacitor must be able to sustain the ac current (or RMS ripple current):

$$I_{OUTac} = \frac{\Delta I_L}{2\sqrt{3}} \quad (\text{eq. 4})$$

Typically, with the recommended 4.7 μH inductor, two ceramic capacitors of 10 μF each in parallel give very good results.

Freewheeling diode:

The diode must be chosen according to its maximum current and voltage ratings, and to thermal considerations.

As far as max ratings are concerned, the maximum reverse voltage the diode sees is the maximum input voltage (with some margin in case of ringing on the Switch node), and the maximum forward current the peak current limit of the NCV890131, I_{LIM} .

The power dissipated in the diode is P_{Dloss} :

$$P_{Dloss} = I_{OUT} \cdot \left(1 - \frac{V_{OUT}}{V_{IN}}\right) \cdot V_F + I_{DRMS} \cdot R_D \quad (\text{eq. 5})$$

with:

- I_{OUT} the average (dc) output current
- V_F the forward voltage of the diode
- I_{DRMS} the RMS current in the diode:

$$I_{DRMS} = \sqrt{(1 - D) \left(I_{OUT}^2 + \frac{\Delta I_L^2}{12} \right)} \quad (\text{eq. 6})$$

- R_D the dynamic resistance of the diode (extracted from the V/I curve of the diode in its datasheet).

Then, knowing the thermal resistance of the package and the amount of heatsinking on the PCB, the temperature rise corresponding to this power dissipation can be estimated.

Input capacitor:

The input capacitor must sustain the RMS input ripple current I_{INac} :

$$I_{INac} = \frac{\Delta I_L}{2} \sqrt{\frac{D}{3}} \quad (\text{eq. 7})$$

It can be designed in combination with an inductor to build an input filter to filter out the ripple current in the source, in order to reduce EMI conducted emissions.

For example, using a 4.7 μH input capacitor, it is easy to calculate that an inductor of 200 nH will ensure that the input filter has a cut-off frequency below 200 kHz (low enough to attenuate the 2 MHz ripple).

PCB LAYOUT RECOMMENDATION

As with any switching power supplies, there are some guidelines to follow to optimize the layout of the printed circuit board for the NCV890131. However, because of the high switching frequency extra care has to be taken.

- Minimize the area of the power current loops:
 - ♦ Input capacitor → NCV890131 switch → Inductor → output capacitor → return through Ground
 - ♦ Freewheeling diode → inductor → Output capacitor → return through ground
- Minimize the length of high impedance signals, and route them far away from the power loops:
 - ♦ Feedback trace
 - ♦ Comp trace

ORDERING INFORMATION

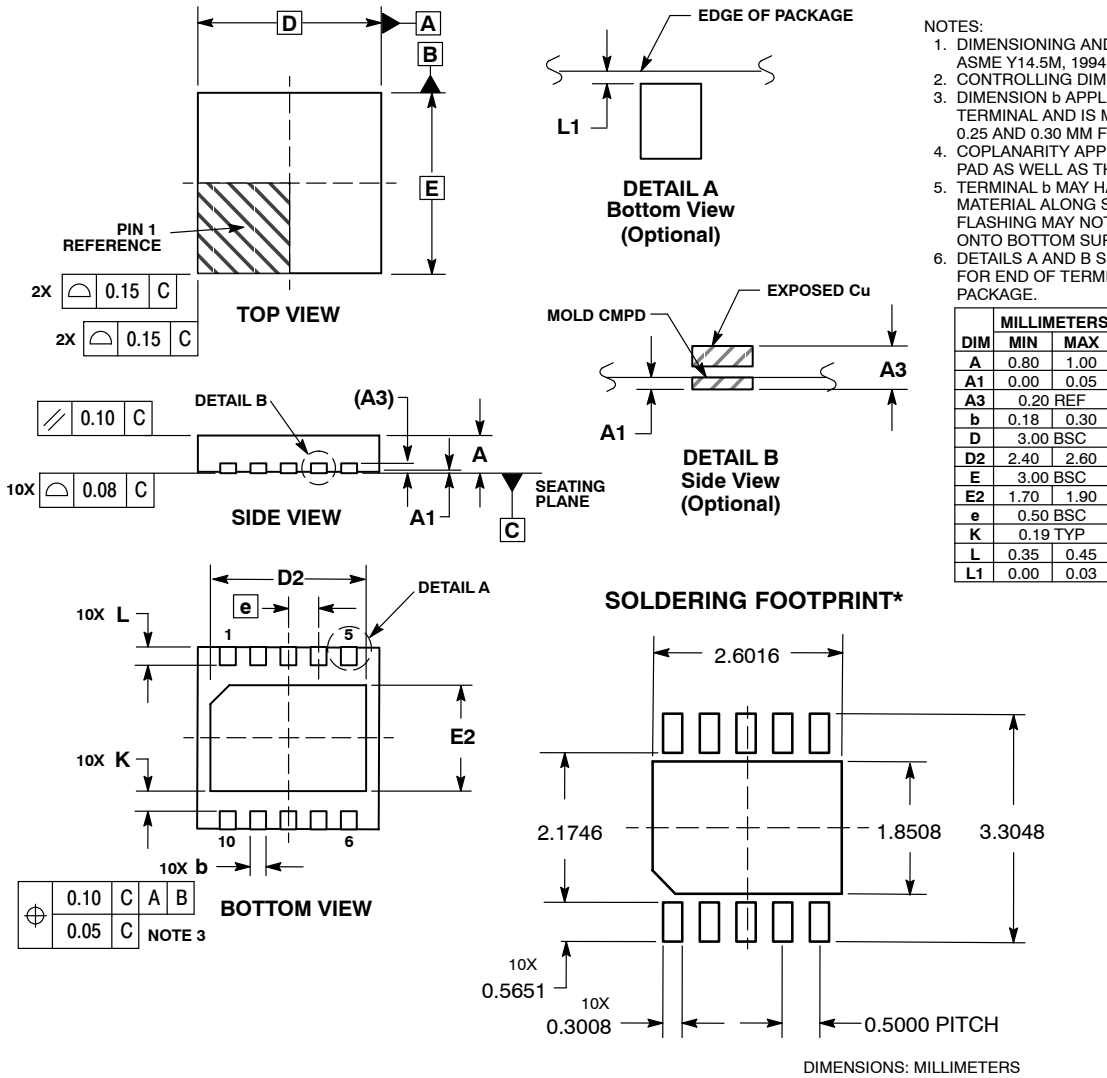
Device	Package	Shipping†
NCV890131MWTXG	DFN10 with wettable flanks (Pb-Free)	3000 / Tape & Reel

†For information on tape and reel specifications, including part orientation and tape sizes, please refer to our Tape and Reel Packaging Specifications Brochure, BRD8011/D.

NCV890131

PACKAGE DIMENSIONS

DFN10, 3x3, 0.5P CASE 485C ISSUE B



- NOTES:
1. DIMENSIONING AND TOLERANCING PER ASME Y14.5M, 1994.
 2. CONTROLLING DIMENSION: MILLIMETERS.
 3. DIMENSION b APPLIES TO PLATED TERMINAL AND IS MEASURED BETWEEN 0.25 AND 0.30 MM FROM TERMINAL.
 4. COPLANARITY APPLIES TO THE EXPOSED PAD AS WELL AS THE TERMINALS.
 5. TERMINAL b MAY HAVE MOLD COMPOUND MATERIAL ALONG SIDE EDGE. MOLD FLASHING MAY NOT EXCEED 30 MICRONS ONTO BOTTOM SURFACE OF TERMINAL b.
 6. DETAILS A AND B SHOW OPTIONAL VIEWS FOR END OF TERMINAL LEAD AT EDGE OF PACKAGE.

*For additional information on our Pb-Free strategy and soldering details, please download the ON Semiconductor Soldering and Mounting Techniques Reference Manual, SOLDERRM/D.

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