



#### Slew Rate Controlled Load Switch

### **General Description**

The AAT4250 SmartSwitch is a member of Skyworks' Application Specific Power MOSFET (ASPM<sup>TM</sup>) product family. It is a slew rate controlled P-channel MOSFET power switch designed for high-side load switching applications. This switch operates with an input voltage range from 1.8V to 5.5V, making it ideal for 2.5V, 3.3V, or 5V systems. The part features 1.5ms turn-on and 10µs turn-off time. The AAT4250 has an under-voltage lockout which turns off the switch when an under-voltage condition exists. Input logic levels are TTL compatible. The quiescent supply current is very low, typically 2µA. In shutdown mode, the supply current is typically reduced to 0.1µA or less.

The AAT4250 is available in a Pb-free, 5-pin SOT23 (SOT25) package or a Pb-free, 8-pin SC70JW package and is specified over the  $-40^{\circ}$ C to  $+85^{\circ}$ C temperature range.

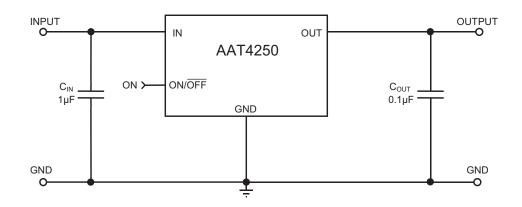
#### Features

- 1.8V to 5.5V Input Voltage Range
- 120m $\Omega$  (5V) Typical R<sub>DS(ON)</sub>
- Low Quiescent Current:
  - Typical 2µA
  - Typical 0.1µA with Enable Off
- Only 2.0V Needed for ON/OFF Control
- Temperature Range: -40°C to +85°C
- 5kV ESD Rating
- SOT23-5 or SC70JW-8 Package

### Applications

- Hot Swap Supplies
- Notebook Computers
- Personal Communication Devices

## **Typical Application**



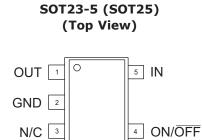


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# **Pin Descriptions**

P	in #			
SOT23-5	SC70JW-8	Symbol	Function	
1	1	OUT	P-channel MOSFET drain.	
2	2, 3, 4, 5	GND	GND Ground connection.	
3	N/A	N/C	N/C Not internally connected.	
4	6	ON/OFF	FF Active-high enable input. Logic high turns the switch on.	
5	7, 8	IN	P-channel MOSFET source.	

## **Pin Configuration**





OUT I	∎ IN
GND 🗉	IN IN
GND 🗉	ON/OFF
GND 4	5 GND



## Slew Rate Controlled Load Switch

### Absolute Maximum Ratings<sup>1</sup>

 $T_A = 25^{\circ}C$ , unless otherwise noted.

Symbol	Description		Value	Units	
V <sub>IN</sub>	IN to GND	IN to GND		V	
V <sub>on</sub>	ON/OFF to GND		-0.3 to 6	V	
V <sub>OUT</sub>	OUT to GND		-0.3 to V <sub>IN</sub> + 0.3	V	
I <sub>MAX</sub>	Maximum Continuous Switch Current		1.7	A	
т	Maximum Pulsed Current	IN ≥ 2.5V	4	Δ	
I <sub>DM</sub>		IN < 2.5V	2	A	
T <sub>1</sub>	Operating Junction Temperature Range		-40 to 150	°C	
T <sub>LEAD</sub>	Maximum Soldering Temperature (at leads)		300	°C	
V <sub>ESD</sub>	ESD Rating <sup>2</sup> - HBM		5000	V	

## **Thermal Characteristics<sup>3</sup>**

Symbol	Description		Value	Units	
0	Thermal Resistance	SC70JW-8	150	°C/W	
θ <sub>JA</sub>		SOT23-5	233.4	°C/ W	
P <sub>D</sub>	Power Dissipation	SC70JW-8	667	m\\/	
		SOT23-5	428	mW	

1. Stresses above those listed in Absolute Maximum Ratings may cause permanent damage to the device. Functional operation at conditions other than the operating conditions specified is not implied. Only one Absolute Maximum Rating should be applied at any one time.

2. Human body model is a 100pF capacitor discharged through a  $1.5k\Omega$  resistor into each pin.

3. Mounted on an AAT4250 demo board in still 25°C air.



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## **Electrical Characteristics**

 $V_{IN}$  = 5V,  $T_A$  = -40°C to +85°C, unless otherwise noted. Typical values are  $T_A$  = 25°C.

Symbol	Description	Conditions	Min	Тур	Max	Units	
V <sub>IN</sub>	Operation Voltage		1.8 <sup>1</sup>		5.5	V	
I <sub>Q</sub>	Quiescent Current	$V_{IN} = 5V, ON/\overline{OFF} = V_{IN}, I_{OUT} = 0$		2	4	μA	
I <sub>Q(OFF)</sub>	Off Supply Current	$ON/\overline{OFF} = GND, V_{IN} = 5V, OUT Open$			1	μA	
I <sub>SD(OFF)</sub>	Off Switch Current	$ON/\overline{OFF} = GND, V_{IN} = 5V, V_{OUT} = 0$		0.1	1	μA	
V <sub>UVLO</sub>	Under-Voltage Lockout	V <sub>IN</sub> Falling	1.0	1.5	1.8	V	
V <sub>UVLO(hys)</sub>	Under-Voltage Lockout Hysteresis			250		mV	
	On Resistance	$V_{IN} = 5V, T_A = 25^{\circ}C$		120	175	mΩ	
R <sub>DS(ON)</sub>		$V_{IN} = 3V, T_A = 25^{\circ}C$		135	200		
		$V_{IN} = 1.8V$		165			
TC <sub>RDS</sub>	On Resistance Temperature Coefficient			2800		ppm/°C	
VIL	ON/OFF Input Logic Low Voltage	$V_{IN} = 2.7V$ to $5.5V^2$			0.8	V	
V	ON/OFF Input Logic High Voltage	$V_{IN} = 2.7V$ to $\Box 4.2V$	2.0			V	
$V_{IH}$		$V_{IN} = >4.2V$ to 5.5V	2.4				
I <sub>SINK</sub>	ON Input Leakage	$V_{ON} = 5V$		0.01	1	μA	
T <sub>D</sub>	Output Turn-On Delay Time			300		μs	
T <sub>DOFF</sub>	Turn-Off Delay Time	$V_{IN} = 5V, R_{LOAD} = 10\Omega$			10	μs	
		$V_{IN} = 3V, R_{LOAD} = 5\Omega$			10		
		$V_{IN} = 5V, R_{LOAD} = 16.5\Omega, T_A = 0 \text{ to } 50^{\circ}\text{C}$ 1000					
Ton	Turn-On Rise Time	$V_{IN} = 5V, R_{LOAD} = 10\Omega, C_{OUT} = 0.1 \mu F$		1500		μs	
		$V_{IN} = 3V$ , $R_{LOAD} = 5\Omega$ , $C_{OUT} = 0.1 \mu F$		1500			

<sup>1.</sup> Part requires minimum start-up of  $V_{\rm IN} \geq$  2.0V to ensure operation down to 1.8V.

<sup>2.</sup> For  $V_{\ensuremath{\text{IN}}}$  outside this range, consult typical ON/OFF threshold curve.

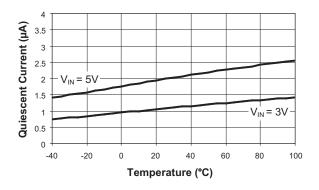


## Slew Rate Controlled Load Switch

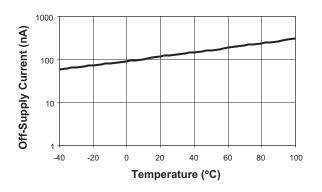
## **Typical Characteristics**

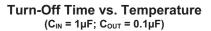
Unless otherwise noted,  $V_{IN} = 5V$ ,  $T_A = 25^{\circ}C$ .

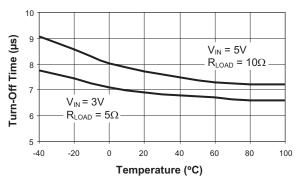
#### Quiescent Current vs. Temperature



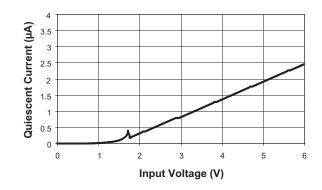
**Off-Supply Current vs. Temperature** 



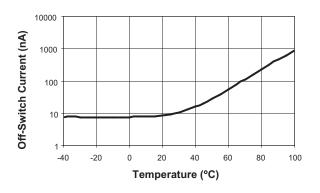


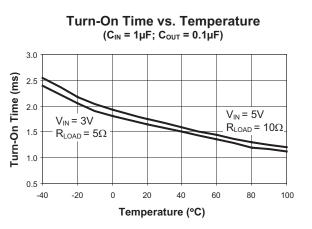


**Quiescent Current vs. Input Voltage** 



**Off-Switch Current vs. Temperature** 



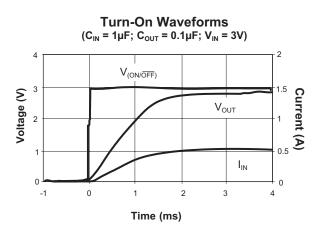


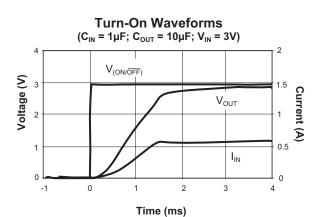


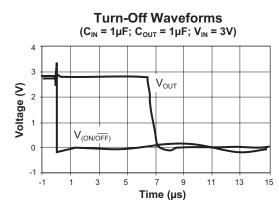
## Slew Rate Controlled Load Switch

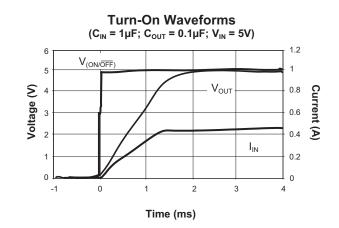
# **Typical Characteristics**

Unless otherwise noted,  $V_{IN} = 5V$ ,  $T_A = 25^{\circ}C$ .



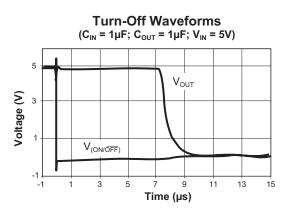






**Turn-On Waveforms**  $(C_{IN} = 1\mu F; C_{OUT} = 10\mu F; V_{IN} = 5V)$ 1.2 6  $V_{(\text{ON/OFF})}$ 5 1 Current Voltage (V) 0.8 4 V<sub>OUT</sub> 0.6 3 0.4 > 2  $\mathbf{I}_{\mathrm{IN}}$ 0.2 1 0 0 3 -1 0 1 2 4







 $I_{OUT} = 100 \text{mA}$ 

4.5

5

5.5

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R<sub>DS(ON)</sub> vs. Input Voltage

190

180

170

160

150

140

130

120

110

1.5

2

2.5

3

3.5

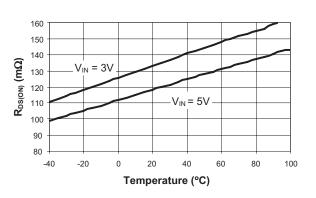
Input Voltage (V)

4

 $R_{DS(ON)}$  (m $\Omega$ )

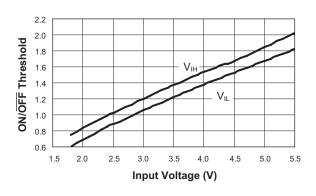
# **Typical Characteristics**

Unless otherwise noted,  $V_{IN}$  = 5V,  $T_A$  = 25°C.



#### R<sub>DS(ON)</sub> vs. Temperature

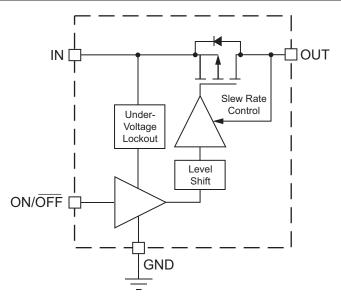






### Slew Rate Controlled Load Switch

#### **Functional Block Diagram**



### **Functional Description**

The AAT4250 is a slew rate controlled P-channel MOSFET power switch designed for high-side load switching applications. It operates with input voltages ranging from 1.8V to 5.5V which, along with its extremely low operating current, makes it ideal for battery-powered applications. In cases where the input voltage drops below 1.8V, the AAT4250 MOSFET is protected from entering the saturated region of operation by automatically shutting down. In addition, the TTL compatible ON/OFF pin makes the AAT4250 an ideal level-shifted load switch. The slew rate controlling feature eliminates inrush current when the MOSFET is turned on, allowing the AAT4250 to be used with a small input capacitor, or no input capacitor at all. During slewing, the current ramps linearly until it reaches the level required for the output load condition. The proprietary control method works by careful control and monitoring of the MOSFET gate voltage. When the device is switched ON, the gate voltage is quickly increased to the threshold level of the MOSFET. Once at this level, the current begins to slew as the gate voltage is slowly increased until the MOSFET becomes fully enhanced. Once it has reached this point, the gate is quickly increased to the full input voltage and  $R_{DS(ON)}$  is minimized.

## **Applications Information**

#### **Input Capacitor**

A 1µF or larger capacitor is typically recommended for  $C_{IN}$  in most applications. A  $C_{IN}$  capacitor is not required for basic operation; however, it is useful in preventing load transients from affecting upstream circuits.  $C_{IN}$  should be located as close to the device  $V_{IN}$  pin as practically possible. Ceramic, tantalum, or aluminum electrolytic capacitors may be selected for  $C_{IN}$ . There is no specific capacitor equivalent series resistance (ESR) requirement for  $C_{IN}$ . However, for higher current operation, ceramic capacitors are recommended for  $C_{IN}$  due to their inherent capability over tantalum capacitors to withstand input current surges from low-impedance sources, such as batteries in portable devices.

#### **Output Capacitor**

For proper slew operation, a  $0.1\mu F$  capacitor or greater is required between  $V_{\mbox{\scriptsize OUT}}$  and GND.

Likewise, with the output capacitor, there is no specific capacitor ESR requirement. If desired,  $C_{OUT}$  may be increased without limit to accommodate any load transient condition without adversely affecting the slew rate.

**AAT**4250

### Slew Rate Controlled Load Switch

#### **Enable Function**

The AAT4250 features an enable / disable function. This pin (ON) is active high and is compatible with TTL or CMOS logic. To assure the load switch will turn on, the ON control level must be greater than 2.0V. The load switch will go into shutdown mode when the voltage on the ON pin falls below 0.8V. When the load switch is in shutdown mode, the OUT pin is tri-stated, and quiescent current drops to leakage levels below  $1\mu$ A.

#### Reverse Output-to-Input Voltage Conditions and Protection

Under normal operating conditions, a parasitic diode exists between the output and input of the load switch. The input voltage should always remain greater than the output load voltage, maintaining a reverse bias on the internal parasitic diode. Conditions where  $V_{OUT}$  might exceed  $V_{IN}$  should be avoided since this would forward bias the internal parasitic diode and allow excessive current flow into the  $V_{OUT}$  pin, possibly damaging the load switch.

In applications where there is a possibility of  $V_{\text{OUT}}$  exceeding  $V_{\text{IN}}$  for brief periods of time during normal operation, the use of a larger value  $C_{\text{IN}}$  capacitor is highly recommended. A larger value of  $C_{\text{IN}}$  with respect to  $C_{\text{OUT}}$  will effect a slower  $C_{\text{IN}}$  decay rate during shutdown, thus preventing  $V_{\text{OUT}}$  from exceeding  $V_{\text{IN}}$ . In applications where there is a greater danger of  $V_{\text{OUT}}$  exceeding  $V_{\text{IN}}$  for extended periods of time, it is recommended to place a Schottky diode from  $V_{\text{IN}}$  to  $V_{\text{OUT}}$  (connecting the cathode to  $V_{\text{IN}}$  and anode to  $V_{\text{OUT}}$ ). The Schottky diode forward voltage should be less than 0.45V.

#### Thermal Considerations and High Output Current Applications

The AAT4250 is designed to deliver a continuous output load current. The limiting characteristic for maximum safe operating output load current is package power dissipation. In order to obtain high operating currents, careful device layout and circuit operating conditions must be taken into account.

The following discussions will assume the load switch is mounted on a printed circuit board utilizing the minimum recommended footprint as stated in the Printed Circuit Board Layout Recommendations section of this datasheet.

At any given ambient temperature  $(T_A)$ , the maximum package power dissipation can be determined by the following equation:

$$\mathsf{P}_{\mathsf{D}(\mathsf{MAX})} = \frac{\mathsf{T}_{\mathsf{J}(\mathsf{MAX})} - \mathsf{T}_{\mathsf{A}}}{\theta_{\mathsf{J}\mathsf{A}}}$$

Constants for the AAT4250 are maximum junction temperature ( $T_{J(MAX)} = 125^{\circ}$ C) and package thermal resistance ( $\theta_{JA} = 150^{\circ}$ C/W). Worst case conditions are calculated at the maximum operating temperature,  $T_A = 85^{\circ}$ C. Typical conditions are calculated under normal ambient conditions where  $T_A = 25^{\circ}$ C. At  $T_A = 85^{\circ}$ C,  $P_{D(MAX)} = 267$ mW. At  $T_A = 25^{\circ}$ C,  $P_{D(MAX)} = 667$ mW.

The maximum continuous output current for the AAT4250 is a function of the package power dissipation and the  $R_{\text{DS}}$  of the MOSFET at  $T_{J(\text{MAX})}$ . The maximum  $R_{\text{DS}}$  of the MOSFET at  $T_{J(\text{MAX})}$  is calculated by increasing the maximum room temperature  $R_{\text{DS}}$  by the  $R_{\text{DS}}$  temperature coefficient. The temperature coefficient (TC) is 2800ppm/ °C. Therefore, at 125°C:

$$\begin{split} R_{\text{DS(MAX)}} &= R_{\text{DS(25°C)}} \cdot (1 + \text{TC} \cdot \Delta \text{T}) \\ R_{\text{DS(MAX)}} &= 175 \text{m}\Omega \cdot (1 + 0.002800 \cdot (125^{\circ}\text{C} - 25^{\circ}\text{C})) \\ R_{\text{DS(MAX)}} &= 224 \text{m}\Omega \end{split}$$

For maximum current, refer to the following equation:

$$I_{OUT(MAX)} < \frac{P_{D(MAX)}}{R_{DS}}^{\frac{1}{2}}$$

For example, if  $V_{IN} = 5V$ ,  $R_{DS(MAX)} = 224m\Omega$ , and  $T_A = 25^{\circ}$ C,  $I_{OUT(MAX)} = 1.7$ A. If the output load current were to exceed 1.7A or if the ambient temperature were to increase, the internal die temperature would increase and the device would be damaged.

Higher peak currents can be obtained with the AAT4250. To accomplish this, the device thermal resistance must be reduced by increasing the heat sink area or by operating the load switch in a duty-cycle manner. Duty cycles with peaks less than 2ms in duration can be considered using the method below.



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#### **High Peak Output Current Applications**

Some applications require the load switch to operate at a continuous nominal current level with short duration, high-current peaks. Refer to the  $I_{\text{DM}}$  specification in the Absolute Maximum Ratings table to ensure the AAT4250's maximum pulsed current rating is not exceeded. The duty cycle for both output current levels must be taken into account. To do so, first calculate the power dissipation at the nominal continuous current level, and then add the additional power dissipation due to the short duration, high-current peak scaled by the duty factor.

For example, a 4V system using an AAT4250 operates at a continuous 100mA load current level and has short 2A current peaks, as in a GSM application. The current peak occurs for 576µs out of a 4.61ms period.

First, the current duty cycle is calculated:

% Peak Duty Cycle: X/100 = 576µs/4.61ms % Peak Duty Cycle = 12.5%

The load current is 100mA for 87.5% of the 4.61ms period and 2A for 12.5% of the period. Since the Electrical Characteristics do not report  $R_{\text{DS}(\text{MAX})}$  for 4V operation, it must be approximated by consulting the chart of  $R_{\text{DS}(\text{ON})}$  vs.  $V_{\text{IN}}$ . The  $R_{\text{DS}}$  reported for 5V  $R_{\text{DS}}$  can be scaled by the ratio seen in the chart to derive the  $R_{\text{DS}}$  for 4V  $V_{\text{IN}}$ :  $175 \text{m}\Omega \cdot 120 \text{m}\Omega/115 \text{m}\Omega = 183 \text{m}\Omega$ . Derated for temperature:  $183 \text{m}\Omega \cdot (1 + 0.002800 \cdot (125^{\circ}\text{C} - 25^{\circ}\text{C})) = 235 \text{m}\Omega$ . The power dissipation for a 100mA load is calculated as follows:

$$\begin{split} P_{D(MAX)} &= I2_{OUT} \cdot R_{DS} \\ P_{D(100mA)} &= (100mA)2 \cdot 235m\Omega \\ P_{D(100mA)} &= 2.35mW \end{split}$$

$$\begin{split} P_{D(87.5\%D/C)} &= \ \% DC \cdot P_{D(100mA)} \\ P_{D(87.5\%D/C)} &= \ 0.875 \cdot 2.35mW \\ P_{D(87.5\%D/C)} &= \ 2.1mW \end{split}$$

The power dissipation for 100mA load at 87.5% duty cycle is 2.1mW. Now the power dissipation for the remaining 12.5% of the duty cycle at 2A is calculated:

 $P_{D(MAX)} = I2_{OUT} \cdot R_{DS}$  $P_{D(2A)} = (2A)2 \cdot 235m\Omega$  $P_{D(2A)} = 940mW$ 

$$\begin{split} P_{D(12.5\%D/C)} &= \ \%DC \cdot P_{D(2A)} \\ P_{D(12.5\%D/C)} &= \ 0.125 \cdot 940mW \\ P_{D(12.5\%D/C)} &= \ 117.5mW \end{split}$$

The power dissipation for 2A load at 12.5% duty cycle is 117mW. Finally, the two power figures are summed to determine the total true power dissipation under the varied load.

$$\begin{split} P_{D(total)} &= P_{D(100mA)} + P_{D(2A)} \\ P_{D(total)} &= 2.1mW + 117.5mW \\ P_{D(total)} &= 120mW \end{split}$$

The maximum power dissipation for the AAT4250 operating at an ambient temperature of 85°C is 267mW. The device in this example will have a total power dissipation of 120mW. This is well within the thermal limits for safe operation of the device; in fact, at 85°C, the AAT4250 will handle a 2A pulse for up to 28% duty cycle. At lower ambient temperatures, the duty cycle can be further increased.

#### Printed Circuit Board Layout Recommendations

For proper thermal management, and to take advantage of the low  $R_{\text{DS}(\text{ON})}$  of the AAT4250, a few circuit board layout rules should be followed:  $V_{\text{IN}}$  and  $V_{\text{OUT}}$  should be routed using wider than normal traces, and GND should be connected to a ground plane. For best performance,  $C_{\text{IN}}$  and  $C_{\text{OUT}}$  should be placed close to the package pins.

#### **Evaluation Board Layout**

The AAT4250 evaluation layout follows the printed circuit board layout recommendations, and can be used for good applications layout.

Note: Board layout shown is not to scale.



## Slew Rate Controlled Load Switch

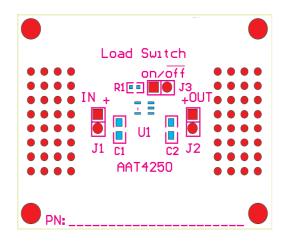


Figure 1: AAT4250 Evaluation Board Top Side Silk Screen Layout / Assembly Drawing.

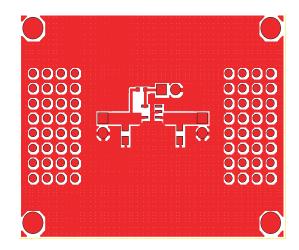


Figure 2: AAT4250 Evaluation Board Component Side Layout.

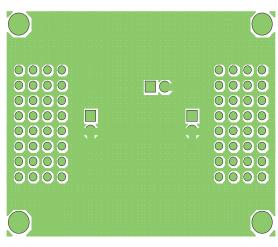


Figure 3: AAT4250 Evaluation Board Solder Side Layout.



# Slew Rate Controlled Load Switch

## **Ordering Information**

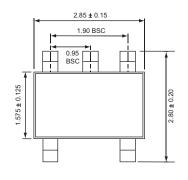
Package	Marking <sup>1</sup>	Part Number (Tape and Reel) <sup>2</sup>
SOT23-5 (SOT25)	ACXYY	AAT4250IGV-T1
SC70JW-8	ACXYY	AAT4250IJS-T1

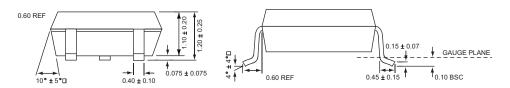


Skyworks Green<sup>TM</sup> products are compliant with all applicable legislation and are halogen-free. For additional information, refer to *Skyworks Definition of Green<sup>TM</sup>*, document number SQ04-0074.

## **Package Information**

SOT23-5 (SOT25)





All dimensions in millimeters.

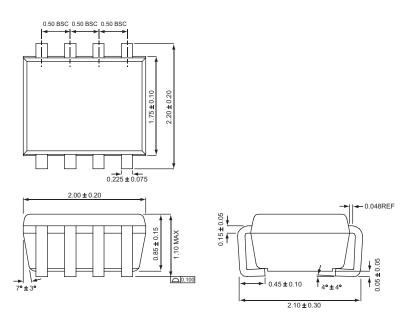
1. XYY = assembly and date code.

2. Sample stock is generally held on part numbers listed in BOLD.



#### Slew Rate Controlled Load Switch

SC70JW-8



All dimensions in millimeters.

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