

# TLV277x-EP, TLV277xA-EP

## FAMILY OF 2.7-V HIGH-SLEW-RATE RAIL-TO-RAIL OUTPUT OPERATIONAL AMPLIFIERS WITH SHUTDOWN

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- **Controlled Baseline**
  - One Assembly/Test Site, One Fabrication Site
- **Extended Temperature Performance of –55°C to 125°C**
- **Enhanced Diminishing Manufacturing Sources (DMS) Support**
- **Enhanced Product-Change Notification**
- **Qualification Pedigree<sup>(1)</sup>**
- **ESD Protection Exceeds 2000 V Per MIL-STD-883, Method 3015; Exceeds 200 V Using Machine Model (C = 200 pF, R = 0)**
- **High Slew Rate . . . 10.5 V/μs Typ**
- **High-Gain Bandwidth . . . 5.1 MHz Typ**
- **Supply Voltage Range 2.5 V to 5.5 V**
- **Rail-to-Rail Output**
- **360 μV Input Offset Voltage**
- **Low Distortion Driving 600-Ω 0.005% THD+N**
- **1 mA Supply Current (Per Channel)**
- **17 nV/√Hz Input Noise Voltage**
- **2 pA Input Bias Current**
- **Characterized From T<sub>A</sub> = –55°C to 125°C**
- **Micropower Shutdown Mode . . . I<sub>DD</sub> < 1 μA**

<sup>†</sup> Component qualification in accordance with JEDEC and industry standards to ensure reliable operation over an extended temperature range. This includes, but is not limited to, Highly Accelerated Stress Test (HAST) or biased 85/85, temperature cycle, autoclave or unbiased HAST, electromigration, bond intermetallic life, and mold compound life. Such qualification testing should not be viewed as justifying use of this component beyond specified performance and environmental limits.

### description

The TLV277x CMOS operational amplifier family combines high slew rate and bandwidth, rail-to-rail output swing, high output drive, and excellent dc precision. The device provides 10.5 V/μs of slew rate and 5.1 MHz of bandwidth while only consuming 1 mA of supply current per channel. This ac performance is much higher than current competitive CMOS amplifiers. The rail-to-rail output swing and high output drive make these devices a good choice for driving the analog input or reference of analog-to-digital converters (ADCs). These devices also have low distortion while driving a 600-Ω load for use in telecom systems.

These amplifiers have a 360-μV input offset voltage, a 17 nV/√Hz input noise voltage, and a 2-pA input bias current for measurement, medical, and industrial applications. The TLV277x family is also specified across an extended temperature range (–55°C to 125°C), making it useful for military and avionics systems.

These devices operate from a 2.5-V to 5.5-V single supply voltage and are characterized at 2.7 V and 5 V. The single-supply operation and low power consumption make these devices a good solution for portable applications. The following table lists the packages available.

FAMILY PACKAGE TABLE

DEVICE	NUMBER OF CHANNELS	PACKAGE TYPES		SHUTDOWN	UNIVERSAL EVM BOARD
		SOIC	TSSOP		
TLV2770	1	8	—	Yes	See the EVM Selection Guide (SLOU060)
TLV2771	1	8	—	—	
TLV2772	2	8	8	—	
TLV2773	2	14	—	Yes	
TLV2774	4	14	14	—	
TLV2775	4	16	16	Yes	



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## SELECTION OF SINGLE-SUPPLY OPERATIONAL AMPLIFIER PRODUCTS†

DEVICE	V <sub>DD</sub> (V)	BW (MHz)	SLEW RATE (V/μs)	I <sub>DD</sub> (per channel) (μA)	RAIL-TO-RAIL
TLV277X	2.5 to 6	5.1	10.5	1000	O
TLV247X	2.7 to 6	2.8	1.5	600	I/O
TLV245X	2.7 to 6	0.22	0.11	23	I/O
TLV246X	2.7 to 6	6.4	1.6	550	I/O

† All specifications measured at 5 V.

## ORDERING INFORMATION†

T <sub>A</sub>	V <sub>IO</sub> MAX AT 25°C (mV)	PACKAGE‡		ORDERABLE PART NUMBER	TOP SIDE MARKING
-55°C to 125°C	2.5	SOIC (D)	Tape and reel	TLV2770MDREP§	
	1.6	SOIC (D)	Tape and reel	TLV2770AMDREP§	
	2.5	SOIC (D)	Tape and reel	TLV2771MDREP§	
	1.6	SOIC (D)	Tape and reel	TLV2771AMDREP§	
	2.5	SOIC (D)	Tape and reel	TLV2772MDREP§	
		TSSOP (PW)	Tape and reel	TLV2772MPWREP§	
	1.6	SOIC (D)	Tape and reel	TLV2772AMDREP	2772AE
		TSSOP (PW)	Tape and reel	TLV2772AMPWREP§	
	2.5	SOIC (D)	Tape and reel	TLV2773MDREP§	
	1.6	SOIC (D)	Tape and reel	TLV2773AMDREP§	
	2.7	SOIC (D)	Tape and reel	TLV2774MDREP	2774EP
		TSSOP (PW)	Tape and reel	TLV2774MPWREP§	
	2.1	SOIC (D)	Tape and reel	TLV2774AMDREP	2774AEP
		TSSOP (PW)	Tape and reel	TLV2774AMPWREP§	
	2.7	SOIC (D)	Tape and reel	TLV2775MDREP§	
		TSSOP (PW)	Tape and reel	TLV2775MPWREP§	
	2.1	SOIC (D)	Tape and reel	TLV2775AMDREP§	
		TSSOP (PW)	Tape and reel	TLV2775AMPWREP§	

† For the most current package and ordering information, see the Package Option Addendum at the end of this document, or see the TI website at [www.ti.com](http://www.ti.com).

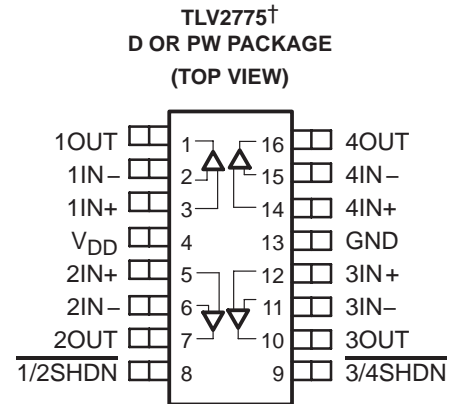
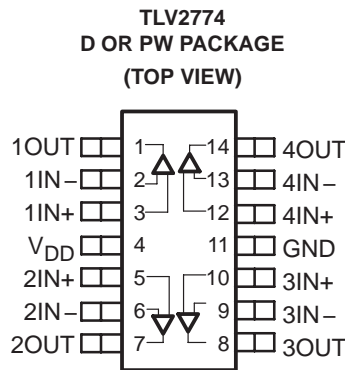
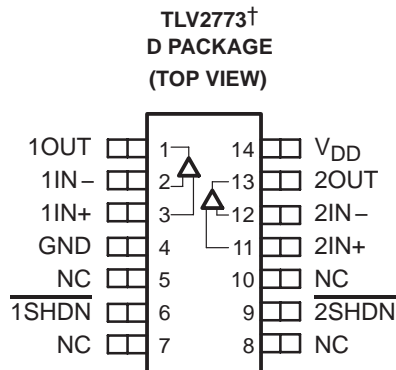
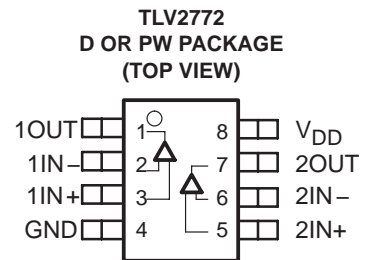
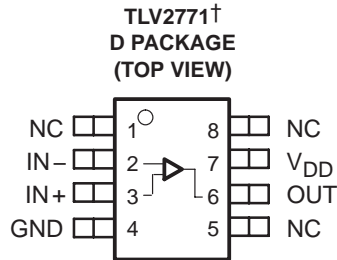
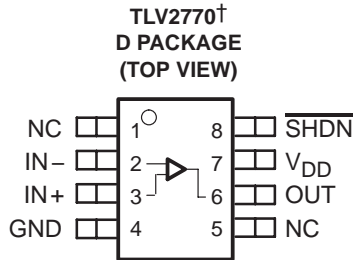
‡ Package drawings, standard packing quantities, thermal data, symbolization, and PCB design guidelines are available at [www.ti.com/packaging](http://www.ti.com/packaging).

§ Product Preview

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## TLV277x PACKAGE PINOUTS



NC – No internal connection

† This device is in the Product Preview stage of development. Please contact your local TI sales office for availability.

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**absolute maximum ratings over operating free-air temperature range (unless otherwise noted)†**

Supply voltage, $V_{DD}$ (see Note 1)	7 V
Differential input voltage, $V_{ID}$ (see Note 2)	$\pm V_{DD}$
Input voltage range, $V_I$ (any input, see Note 1)	-0.3 V to $V_{DD}$
Input current, $I_I$ (any input)	$\pm 4$ mA
Output current, $I_O$	$\pm 50$ mA
Total current into $V_{DD+}$	$\pm 50$ mA
Total current out of GND	$\pm 50$ mA
Duration of short-circuit current (at or below) 25°C (see Note 3)	unlimited
Continuous total power dissipation	See Dissipation Rating Table
Operating free-air temperature range, $T_A$ : M suffix	-55°C to 125°C
Storage temperature range, $T_{stg}$	-65°C to 150°C
Lead temperature 1,6 mm (1/16 inch) from case for 10 seconds	260°C

† Stresses beyond those listed under “absolute maximum ratings” may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those indicated under “recommended operating conditions” is not implied. Exposure to absolute-maximum-rated conditions for extended periods may affect device reliability.

- NOTES: 1. All voltage values, except differential voltages, are with respect to GND.  
 2. Differential voltages are at the noninverting input with respect to the inverting input. Excessive current flows when input is brought below GND - 0.3 V.  
 3. The output may be shorted to either supply. Temperature and/or supply voltages must be limited to ensure that the maximum dissipation rating is not exceeded.

**DISSIPATION RATING TABLE**

PACKAGE	$\theta_{JC}$ (°C/W)		$\theta_{JA}$ (°C/W, 0 AIR FLOW)	
	HIGH K	LOW K	HIGH K	LOW K
D(8)	39.4	42.4	97.1	165.5
D(14)	51.5	53.7	86.2	133.5
D(16)	36.9	38.4	73.1	111.6
PW(8)	65.1	69.4	149.4	230.5
PW(14)	45.8	46.6	111.7	131.4
PW(16)	33.6	35	108.4	147.0

NOTE 4: Thermal resistances are not production tested and are for informational purposes only.

**recommended operating conditions**

	M SUFFIX		UNIT
	MIN	MAX	
Supply voltage, $V_{DD}$	2.5	6	V
Input voltage range, $V_I$	GND	$V_{DD+} - 1.3$	V
Common-mode input voltage, $V_{IC}$	GND	$V_{DD+} - 1.3$	V
Operating free-air temperature, $T_A$	-55	125	°C

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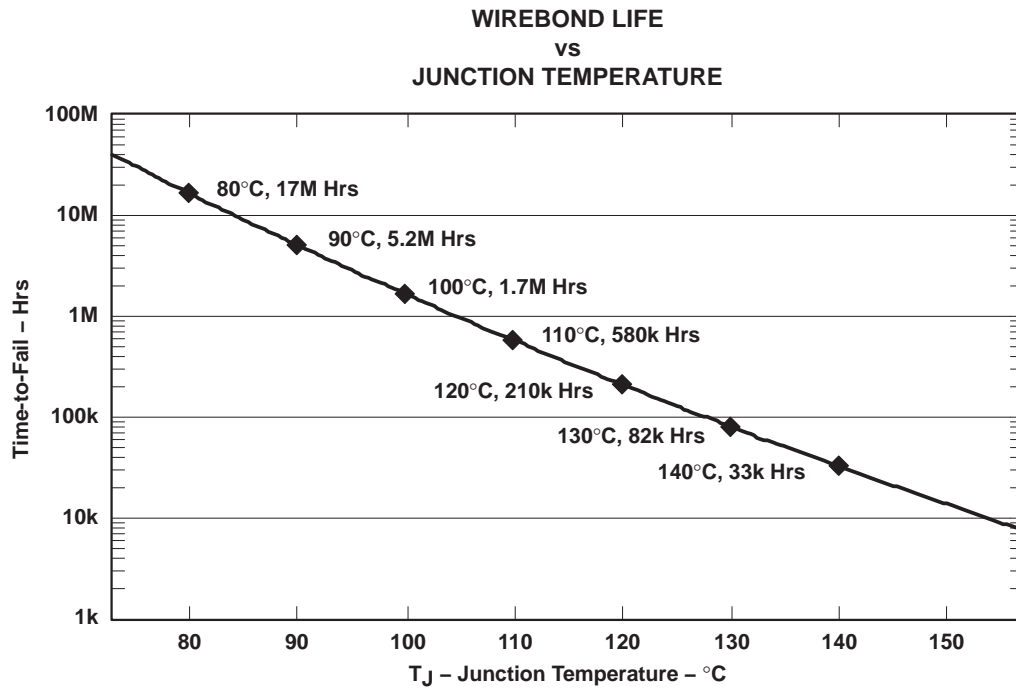


Figure 1. Wirebond Life Estimation

# TLV277x-EP, TLV277xA-EP FAMILY OF 2.7-V HIGH-SLEW-RATE RAIL-TO-RAIL OUTPUT OPERATIONAL AMPLIFIERS WITH SHUTDOWN

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electrical characteristics at specified free-air temperature,  $V_{DD} = 2.7\text{ V}$  (unless otherwise noted)

PARAMETER	TEST CONDITIONS		$T_A$ †	TLV277xM			TLV277xAM			UNIT
				MIN	TYP	MAX	MIN	TYP	MAX	
$V_{IO}$ Input offset voltage	$V_{DD} = \pm 1.35\text{ V}$ , $V_{IC} = 0$ , $V_O = 0$ , $R_S = 50\ \Omega$	TLV2770/1/2/3	25°C	0.44	2.5		0.44	1.6	mV	
			Full range			2.7		1.9		
		TLV2774/5	25°C		0.8	2.7		0.8		2.1
			Full range			3.0				2.4
$\alpha_{VIO}$ Temperature coefficient of input offset voltage	$V_{DD} = \pm 1.35\text{ V}$ , $V_{IC} = 0$ , $V_O = 0$ , $R_S = 50\ \Omega$		25°C to 125°C		2		2		$\mu\text{V}/^\circ\text{C}$	
$I_{IO}$ Input offset current	$V_{DD} = \pm 1.35\text{ V}$ , $V_{IC} = 0$ , $V_O = 0$ , $R_S = 50\ \Omega$	TLV2770/1/2/3	25°C		1	60		1	60	pA
			Full range			125			125	
		TLV2774/5	Full range			200			200	
$I_{IB}$ Input bias current	$V_{DD} = \pm 1.35\text{ V}$ , $V_{IC} = 0$ , $V_O = 0$ , $R_S = 50\ \Omega$	TLV2770/1/2/3	25°C		2	60		2	60	pA
			Full range			350			350	
		TLV2774/5	Full range			500			500	
$V_{ICR}$ Common-mode input voltage range	CMRR > 60 dB, $R_S = 50\ \Omega$		25°C	0 to 1.4	-0.3 to 1.7		0 to 1.4	-0.3 to 1.7	V	
			Full range	0 to 1.4	-0.3 to 1.7		0 to 1.4	-0.3 to 1.7		
$V_{OH}$ High-level output voltage	$I_{OH} = -0.675\text{ mA}$		25°C		2.6		2.6	V		
			Full range		2.45		2.45			
	$I_{OH} = -2.2\text{ mA}$		25°C		2.4		2.4			
			Full range		2.1		2.1			
$V_{OL}$ Low-level output voltage	$V_{IC} = 1.35\text{ V}$ , $I_{OL} = 0.675\text{ mA}$		25°C		0.1		0.1	V		
			Full range			0.2			0.2	
	$V_{IC} = 1.35\text{ V}$ , $I_{OL} = 2.2\text{ mA}$		25°C		0.21		0.21			
			Full range			0.6			0.6	
$A_{VD}$ Large-signal differential voltage amplification	$V_{IC} = 1.35\text{ V}$ , $V_O = 0.6\text{ V to } 2.1\text{ V}$	$R_L = 10\text{ k}\Omega$ ‡	25°C	20	380		20	380	V/mV	
			Full range		13		13			
$r_{i(d)}$ Differential input resistance			25°C		$10^{12}$		$10^{12}$	$\Omega$		
$C_{i(c)}$ Common-mode input capacitance	$f = 10\text{ kHz}$ ,		25°C		8		8	pF		
$Z_o$ Closed-loop output impedance	$f = 100\text{ kHz}$ , $A_V = 10$		25°C		25		25	$\Omega$		
CMRR Common-mode rejection ratio	$V_{IC} = V_{ICR}(\text{min})$ , $R_S = 50\ \Omega$	$V_O = 1.5\text{ V}$	25°C	60	84		60	84	dB	
			Full range		60	82		60		82
$k_{SVR}$ Supply voltage rejection ratio ( $\Delta V_{DD} / \Delta V_{IO}$ )	$V_{DD} = 2.7\text{ V to } 5\text{ V}$ , No load	$V_{IC} = V_{DD}/2$	25°C	70	89		70	89	dB	
			Full range		70	84		70		84
$I_{DD}$ Supply current (per channel)	$V_O = 1.5\text{ V}$ , No load		25°C		1	2		1	2	mA
			Full range			2			2	

† Full range is -55°C to 125°C for M level part.

‡ Referenced to 1.35 V

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operating characteristics at specified free-air temperature,  $V_{DD} = 2.7\text{ V}$  (unless otherwise noted)

PARAMETER	TEST CONDITIONS	$T_A$ †	TLV277xM			TLV277xAM			UNIT		
			MIN	TYP	MAX	MIN	TYP	MAX			
SR	Slew rate at unity gain	$V_{O(PP)} = 0.8\text{ V}$ , $R_L = 10\text{ k}\Omega$	25°C	5	9		5	9	V/ $\mu$ s		
			Full range	4.7	6		4.7	6			
$V_n$	Equivalent input noise voltage	25°C	$f = 1\text{ kHz}$	21			21			nV/ $\sqrt{\text{Hz}}$	
			$f = 10\text{ kHz}$	17			17				
$V_{N(PP)}$	Peak-to-peak equivalent input noise voltage	25°C	$f = 0.1\text{ Hz to }1\text{ Hz}$	0.33			0.33			$\mu$ V	
			$f = 0.1\text{ Hz to }10\text{ Hz}$	0.86			0.86			$\mu$ V	
$I_n$	Equivalent input noise current	25°C	$f = 100\text{ Hz}$	0.6			0.6			fA/ $\sqrt{\text{Hz}}$	
THD + N	Total harmonic distortion plus noise	25°C	$R_L = 600\ \Omega$ , $f = 1\text{ kHz}$	$A_V = 1$	0.0085%			0.0085%			
				$A_V = 10$	0.025%			0.025%			
				$A_V = 100$	0.12%			0.12%			
	Gain-bandwidth product	25°C	$f = 10\text{ kHz}$ , $C_L = 100\text{ pF}$	$R_L = 600\ \Omega$	4.8			4.8			MHz
$t_s$	Settling time	25°C	$A_V = -1$ , Step = 0.85 V to 1.85 V, $R_L = 600\ \Omega$ , $C_L = 100\text{ pF}$	0.1%	0.186			0.186			$\mu$ s
				0.01%	3.92			3.92			
$\phi_m$	Phase margin at unity gain	25°C	$R_L = 600\ \Omega$ , $C_L = 100\text{ pF}$	46°			46°				
	Gain margin	25°C		12			12			dB	

† Full range is  $-55^\circ\text{C}$  to  $125^\circ\text{C}$  for M level part.

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electrical characteristics at specified free-air temperature,  $V_{DD} = 5\text{ V}$  (unless otherwise noted)

PARAMETER	TEST CONDITIONS		$T_A$ †	TLV277xM			TLV277xAM			UNIT
				MIN	TYP	MAX	MIN	TYP	MAX	
$V_{IO}$ Input offset voltage	$V_{DD} = \pm 2.5\text{ V}$ , $V_{IC} = 0$ , $V_O = 0$ , $R_S = 50\ \Omega$	TLV2770/1/2/3	25°C	0.36	2.5		0.36	1.6	mV	
			Full range			2.7		1.9		
		TLV2774/5	25°C		0.8	2.5		0.8		2.1
			Full range			2.7		2.4		
$\alpha_{VIO}$ Temperature coefficient of input offset voltage	$V_{DD} = \pm 2.5\text{ V}$ , $V_{IC} = 0$ , $V_O = 0$ , $R_S = 50\ \Omega$		25°C to 125°C		2		2		$\mu\text{V}/^\circ\text{C}$	
$I_{IO}$ Input offset current	$V_{DD} = \pm 2.5\text{ V}$ , $V_{IC} = 0$ , $V_O = 0$ , $R_S = 50\ \Omega$		25°C		1	60		1	60	pA
			Full range	TLV2770/1/2/3			125		125	
				TLV2774/5			200		200	
$I_{IB}$ Input bias current	$V_{DD} = \pm 2.5\text{ V}$ , $V_{IC} = 0$ , $V_O = 0$ , $R_S = 50\ \Omega$		25°C		2	60		2	60	pA
			Full range	TLV2770/1/2/3			350		350	
				TLV2774/5			500		500	
$V_{ICR}$ Common-mode input voltage range	CMRR > 60 dB, $R_S = 50\ \Omega$		25°C	0 to 3.7	-0.3 to 3.8		0 to 3.7	-0.3 to 3.8	V	
			Full range	0 to 3.7	-0.3 to 3.8		0 to 3.7	-0.3 to 3.8		
$V_{OH}$ High-level output voltage	$I_{OH} = -1.3\text{ mA}$		25°C		4.9		4.9	V		
			Full range		4.8		4.8			
	$I_{OH} = -4.2\text{ mA}$		25°C		4.7		4.7			
			Full range		4.4		4.4			
$V_{OL}$ Low-level output voltage	$V_{IC} = 2.5\text{ V}$ , $I_{OL} = 1.3\text{ mA}$		25°C		0.1		0.1	V		
			Full range		0.2		0.2			
	$V_{IC} = 2.5\text{ V}$ , $I_{OL} = 4.2\text{ mA}$		25°C		0.21		0.21			
			Full range		0.6		0.6			
$A_{VD}$ Large-signal differential voltage amplification	$V_{IC} = 2.5\text{ V}$ , $V_O = 1\text{ V to }4\text{ V}$	$R_L = 10\text{ k}\Omega$ , ‡	25°C	20	450		20	450	V/mV	
			Full range		13		13			
$r_{i(d)}$ Differential input resistance			25°C		1012		1012	$\Omega$		
$C_{i(c)}$ Common-mode input capacitance	$f = 10\text{ kHz}$ ,		25°C		8		8	pF		
$z_o$ Closed-loop output impedance	$f = 100\text{ kHz}$ ,	$A_V = 10$	25°C		20		20	$\Omega$		
CMRR Common-mode rejection ratio	$V_{IC} = V_{ICR}(\text{min})$ , $R_S = 50\ \Omega$	$V_O = 3.7\text{ V}$ ,	25°C	60	96		60	96	dB	
			Full range		60	93		60		93
$k_{SVR}$ Supply voltage rejection ratio ( $\Delta V_{DD}/\Delta V_{IO}$ )	$V_{DD} = 2.7\text{ V to }5\text{ V}$ , No load	$V_{IC} = V_{DD}/2$ ,	25°C	70	89		70	89	dB	
			Full range		70	84		70		84
$I_{DD}$ Supply current (per channel)	$V_O = 1.5\text{ V}$ ,	No load	25°C		1	2		1	2	mA
			Full range			2		2		

† Full range is  $-55^\circ\text{C}$  to  $125^\circ\text{C}$  for M level part.

‡ Referenced to 2.5 V



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operating characteristics at specified free-air temperature,  $V_{DD} = 5\text{ V}$  (unless otherwise noted)

PARAMETER	TEST CONDITIONS	$T_A$ †	TLV277xM			TLV2772xAM			UNIT	
			MIN	TYP	MAX	MIN	TYP	MAX		
SR	Slew rate at unity gain	$V_{O(PP)} = 1.5\text{ V}$ , $C_L = 100\text{ pF}$ , $R_L = 10\text{ k}\Omega$	25°C	5	10.5		5	10.5	V/ $\mu\text{s}$	
			Full range	4.7	6		4.7	6		
$V_n$	Equivalent input noise voltage		25°C	f = 1 kHz			17			nV/ $\sqrt{\text{Hz}}$
				f = 10 kHz			12			
$V_{N(PP)}$	Peak-to-peak equivalent input noise voltage		25°C	f = 0.1 Hz to 1 Hz			0.33			$\mu\text{V}$
				f = 0.1 Hz to 10 Hz			0.86			$\mu\text{V}$
$I_n$	Equivalent input noise current		25°C	f = 100 Hz			0.6			fA/ $\sqrt{\text{Hz}}$
THD + N	Total harmonic distortion plus noise	$R_L = 600\ \Omega$ , f = 1 kHz	25°C	$A_V = 1$			0.005%			
				$A_V = 10$			0.016%			
				$A_V = 100$			0.095%			
	Gain-bandwidth product	f = 10 kHz, $C_L = 100\text{ pF}$	$R_L = 600\ \Omega$ , 25°C	5.1			5.1			MHz
$t_s$	Settling time	$A_V = -1$ , Step = 1.5 V to 3.5 V, $R_L = 600\ \Omega$ , $C_L = 100\text{ pF}$	25°C	0.1%			0.134			$\mu\text{s}$
				0.01%			1.97			
$\phi_m$	Phase margin at unity gain	$R_L = 600\ \Omega$ , $C_L = 100\text{ pF}$	25°C	46°			46°			
	Gain margin		25°C	12			12			dB

† Full range is  $-55^\circ\text{C}$  to  $125^\circ\text{C}$  for M level part.

**TLV277x-EP, TLV277xA-EP**  
**FAMILY OF 2.7-V HIGH-SLEW-RATE RAIL-TO-RAIL OUTPUT**  
**OPERATIONAL AMPLIFIERS WITH SHUTDOWN**

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**TYPICAL CHARACTERISTICS**

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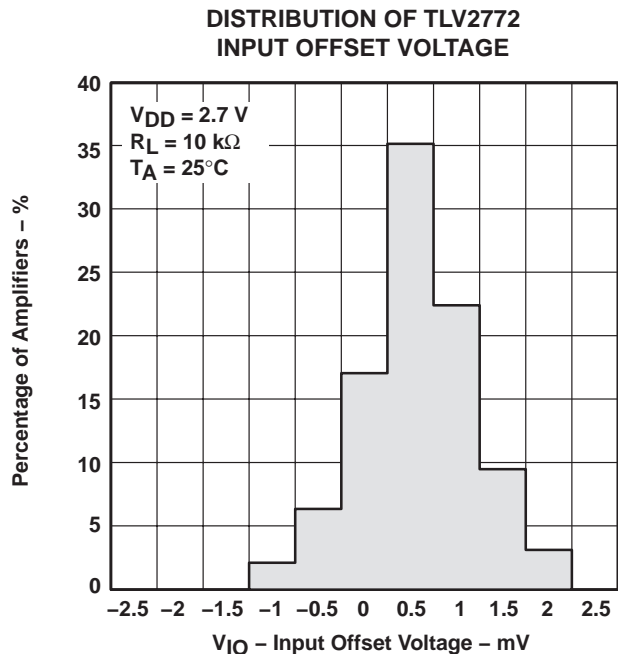
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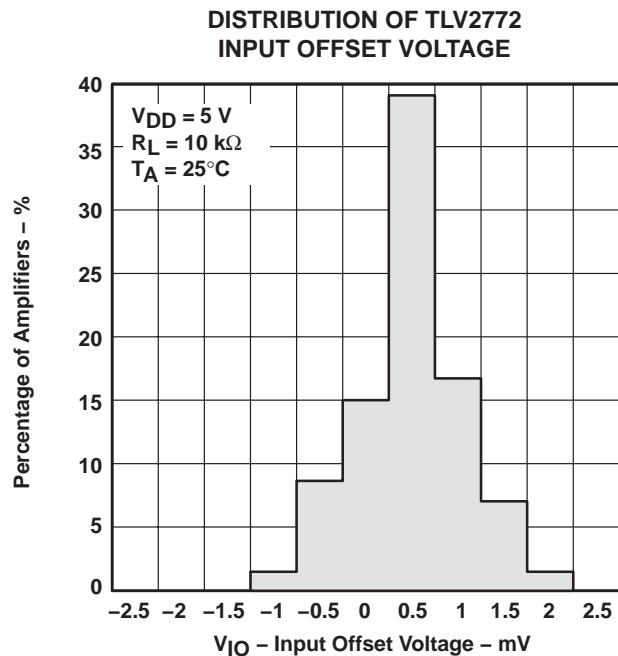
**TLV277x-EP, TLV277xA-EP**  
**FAMILY OF 2.7-V HIGH-SLEW-RATE RAIL-TO-RAIL OUTPUT**  
**OPERATIONAL AMPLIFIERS WITH SHUTDOWN**

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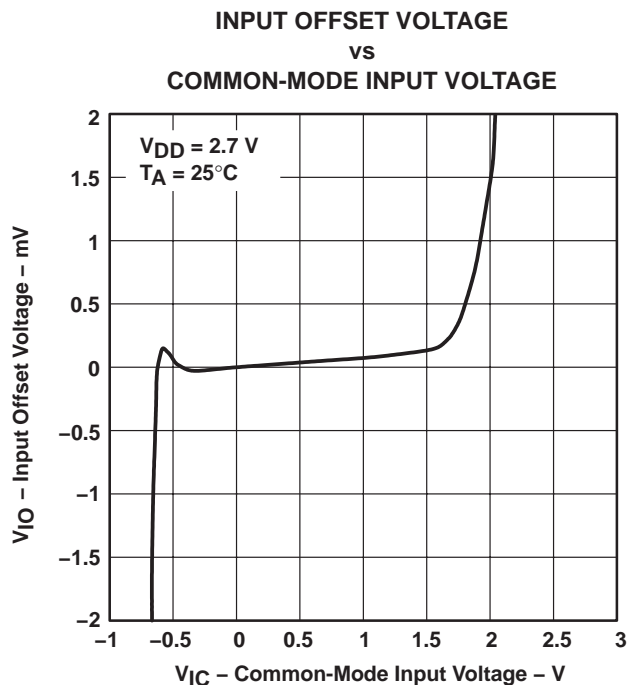
**TYPICAL CHARACTERISTICS**



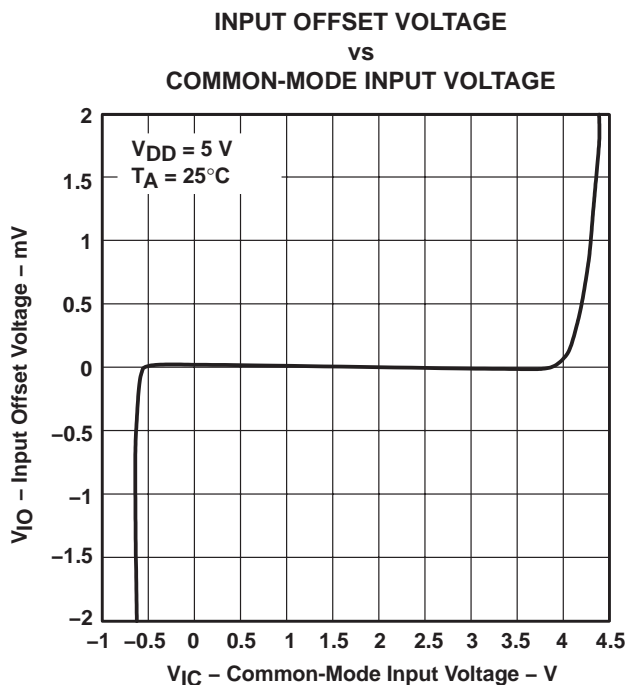
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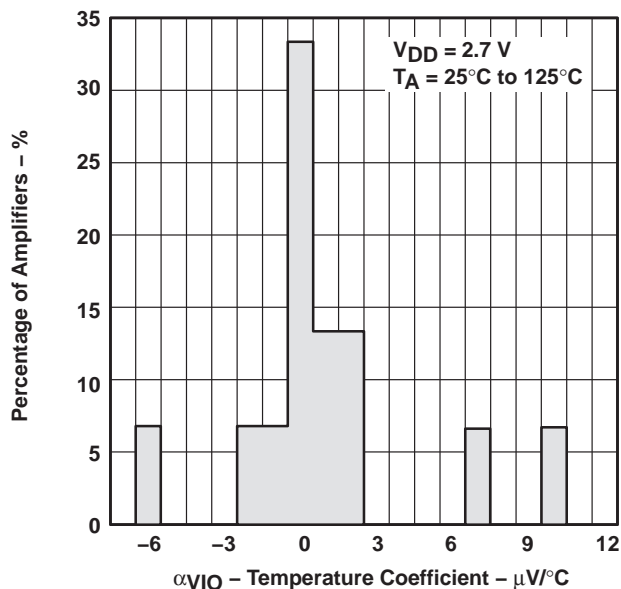
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**TLV277x-EP, TLV277xA-EP**  
**FAMILY OF 2.7-V HIGH-SLEW-RATE RAIL-TO-RAIL OUTPUT**  
**OPERATIONAL AMPLIFIERS WITH SHUTDOWN**

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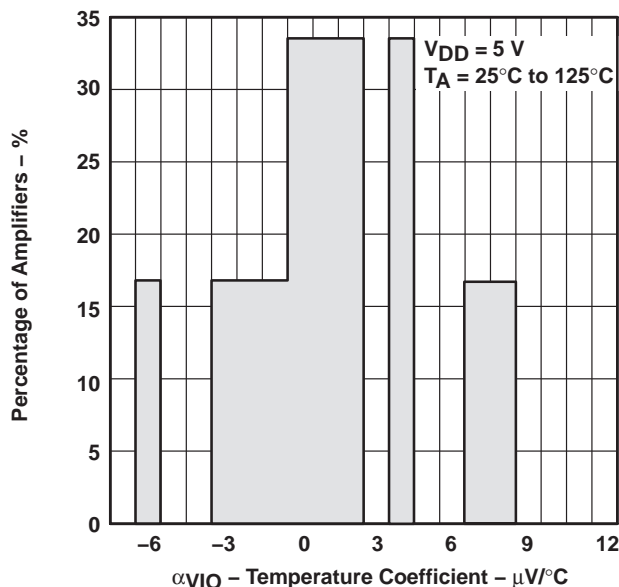
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**DISTRIBUTION OF TLV2772**  
**INPUT OFFSET VOLTAGE**



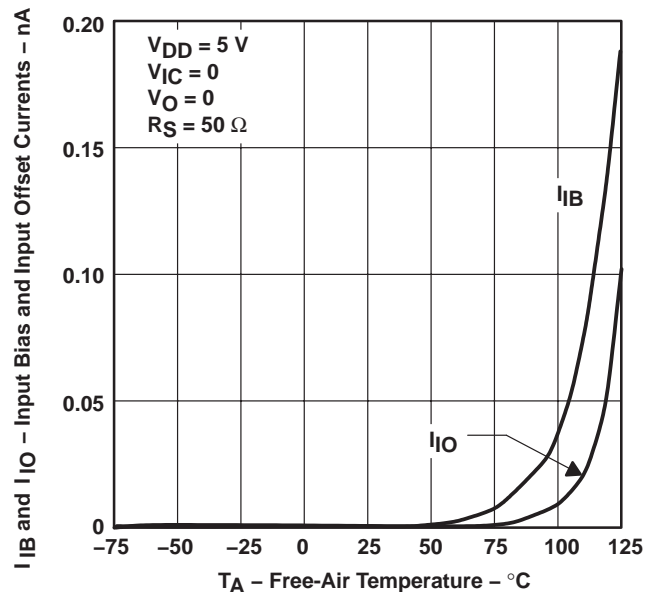
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**DISTRIBUTION OF TLV2772**  
**INPUT OFFSET VOLTAGE**



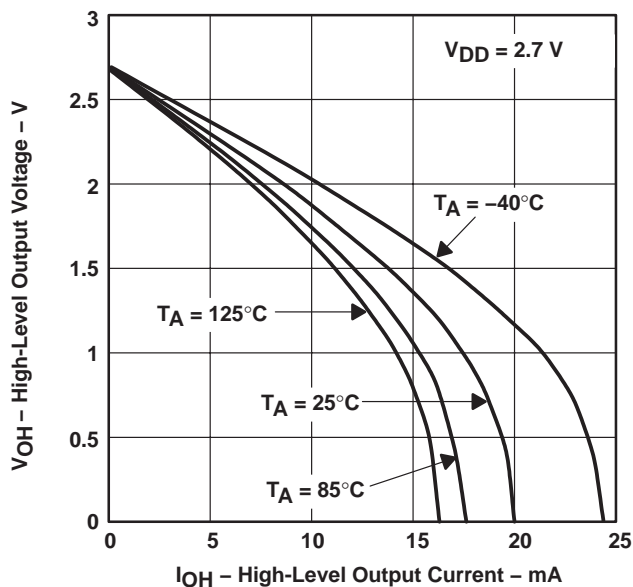
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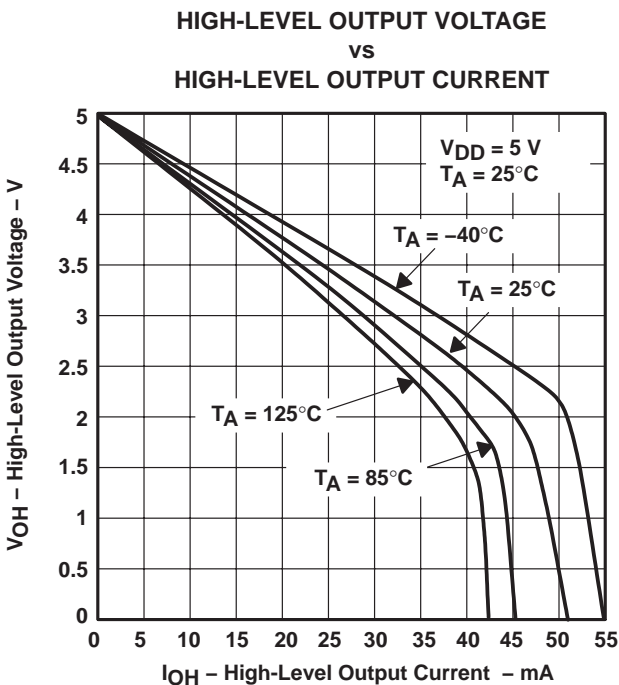
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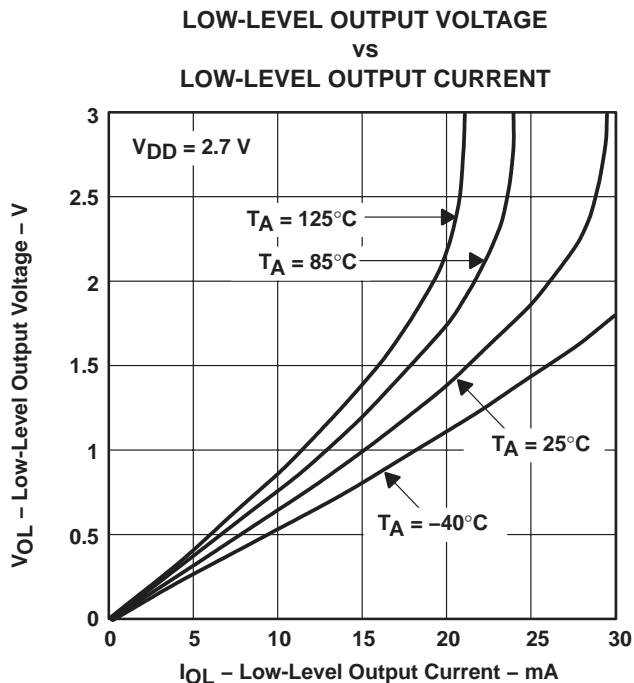
**TLV277x-EP, TLV277xA-EP**  
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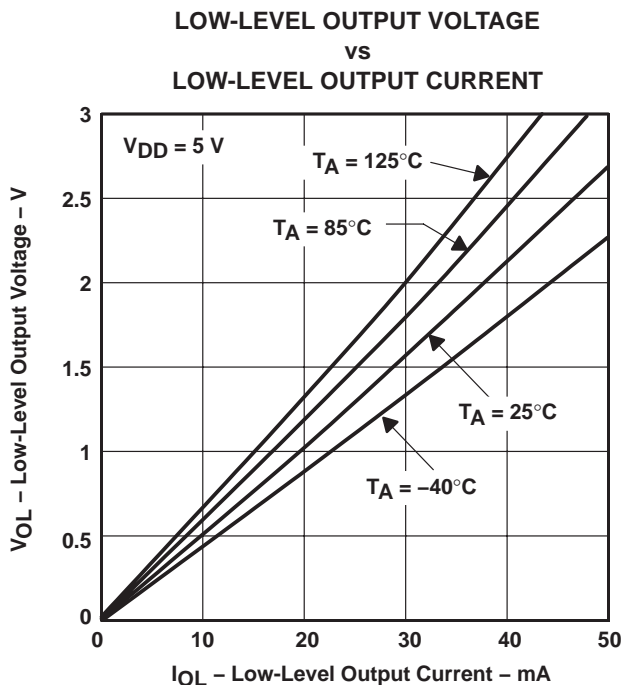
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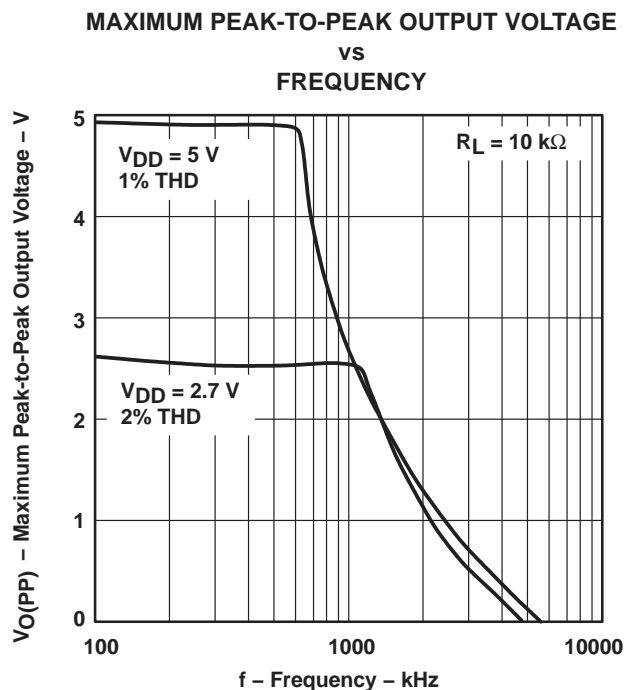
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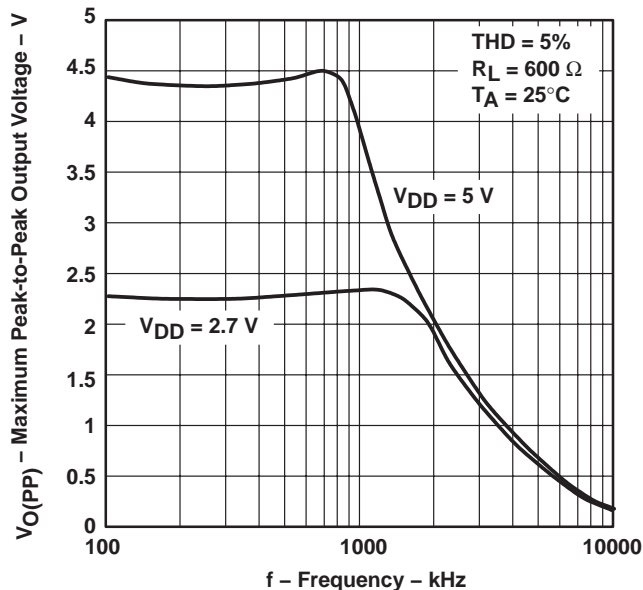
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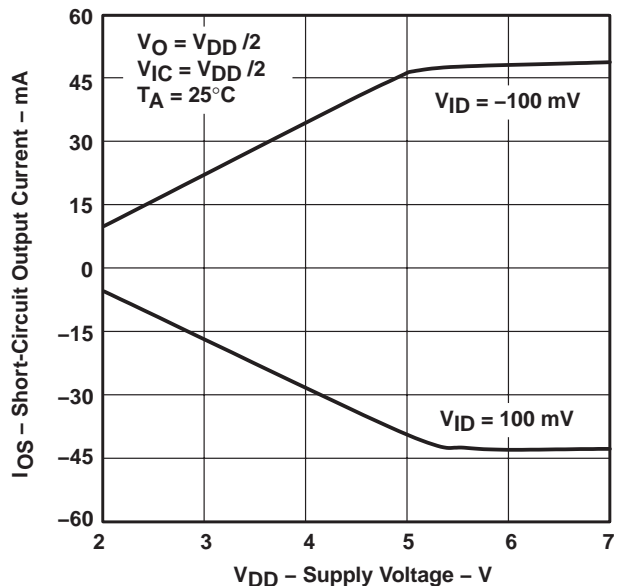
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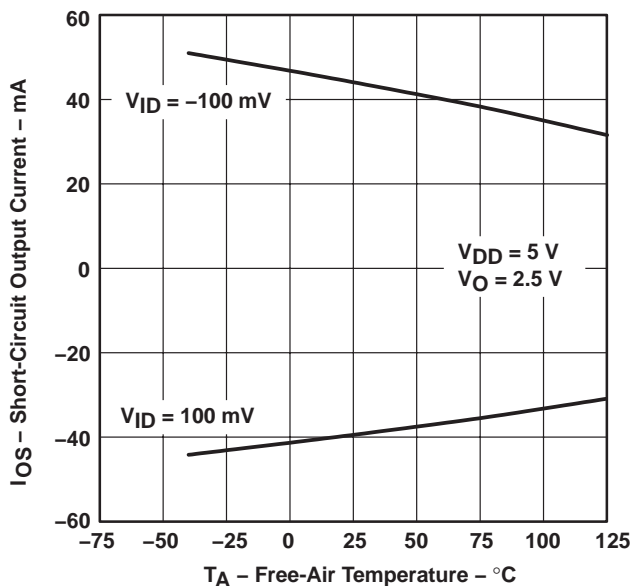
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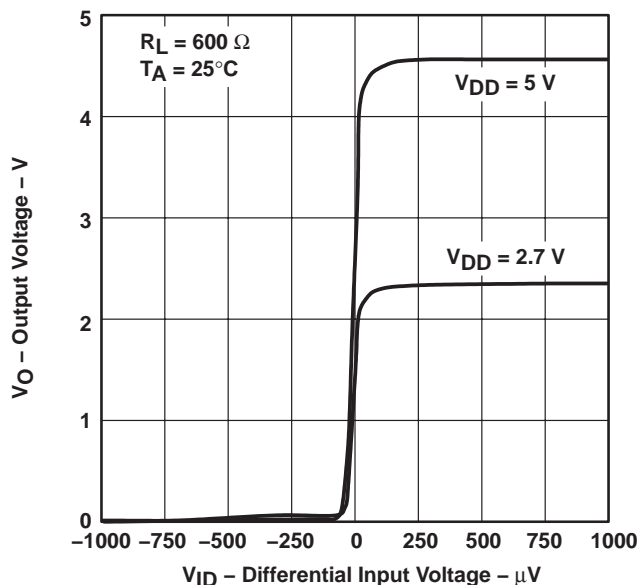
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**OUTPUT VOLTAGE**  
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**TLV277x-EP, TLV277xA-EP**  
**FAMILY OF 2.7-V HIGH-SLEW-RATE RAIL-TO-RAIL OUTPUT**  
**OPERATIONAL AMPLIFIERS WITH SHUTDOWN**

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**TYPICAL CHARACTERISTICS**

**LARGE-SIGNAL DIFFERENTIAL VOLTAGE AMPLIFICATION**  
**AND PHASE MARGIN**

vs  
**FREQUENCY**

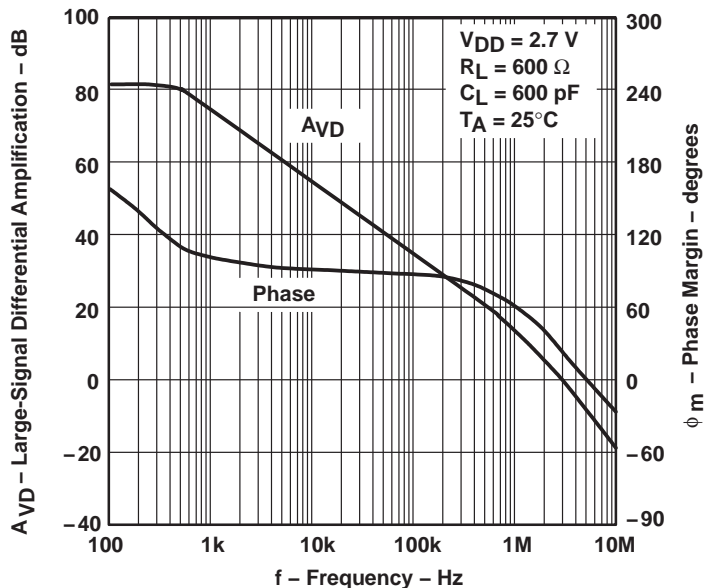


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vs  
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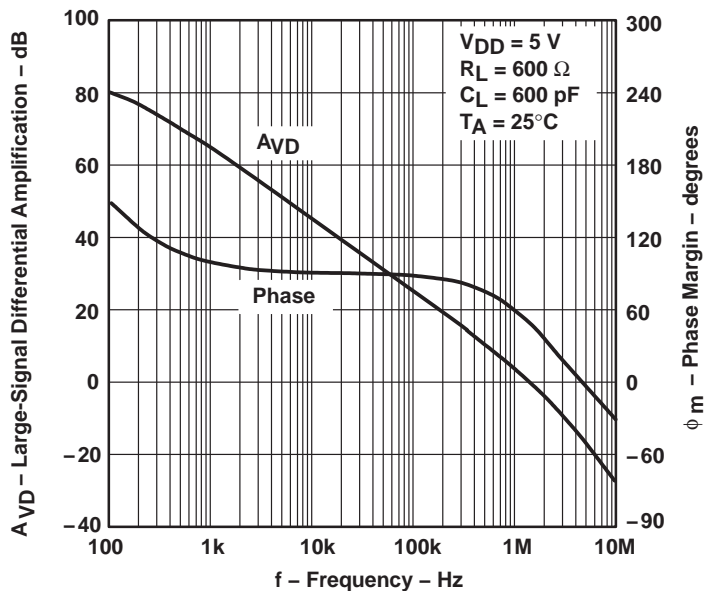


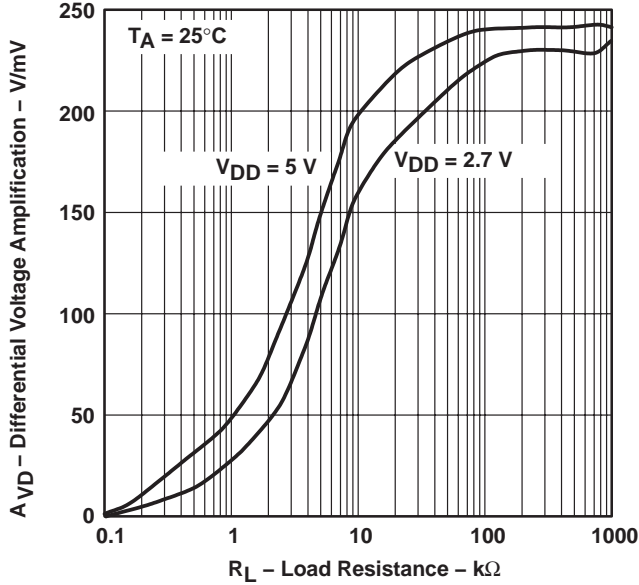
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**FAMILY OF 2.7-V HIGH-SLEW-RATE RAIL-TO-RAIL OUTPUT**  
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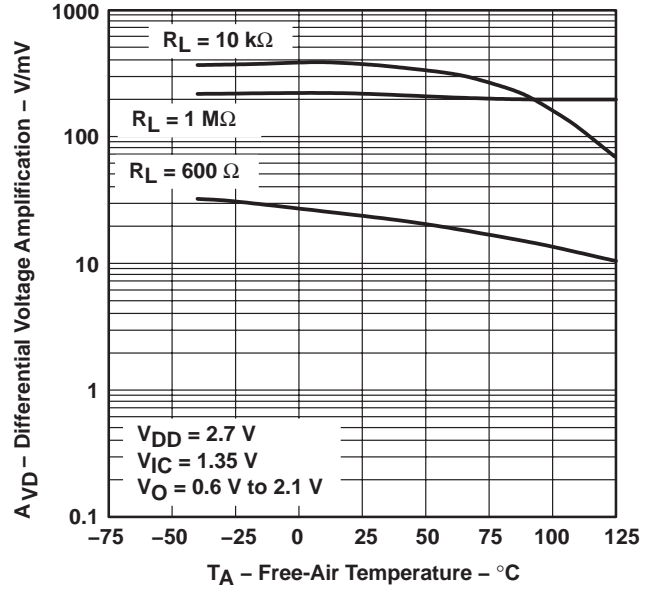
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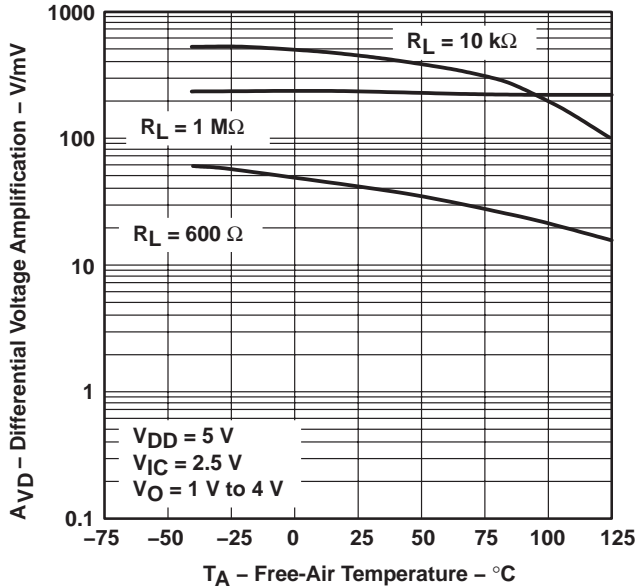
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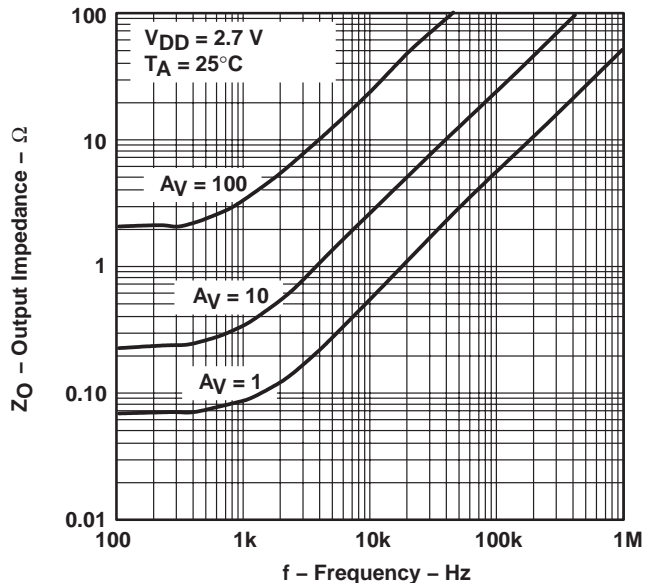
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**Figure 23**





TYPICAL CHARACTERISTICS

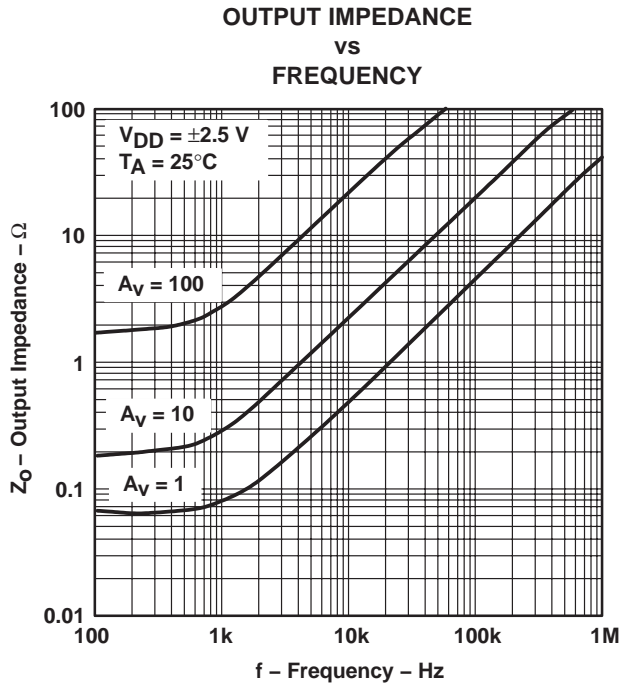


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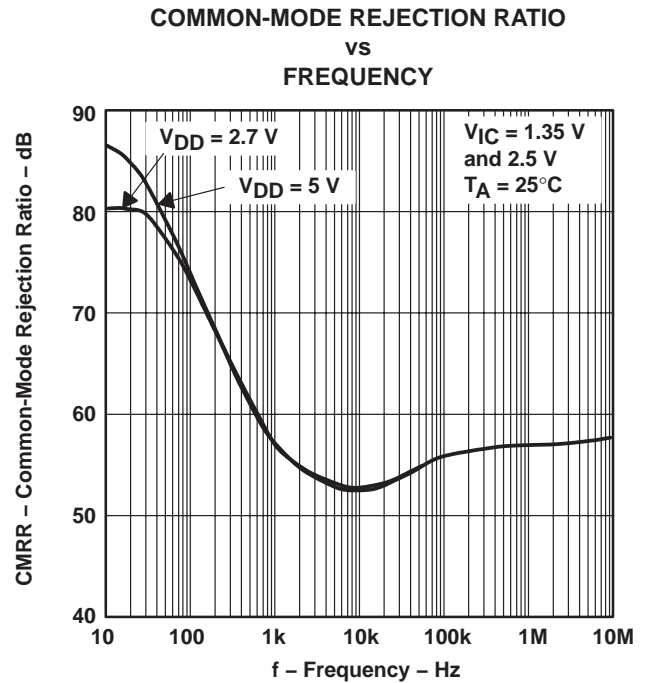


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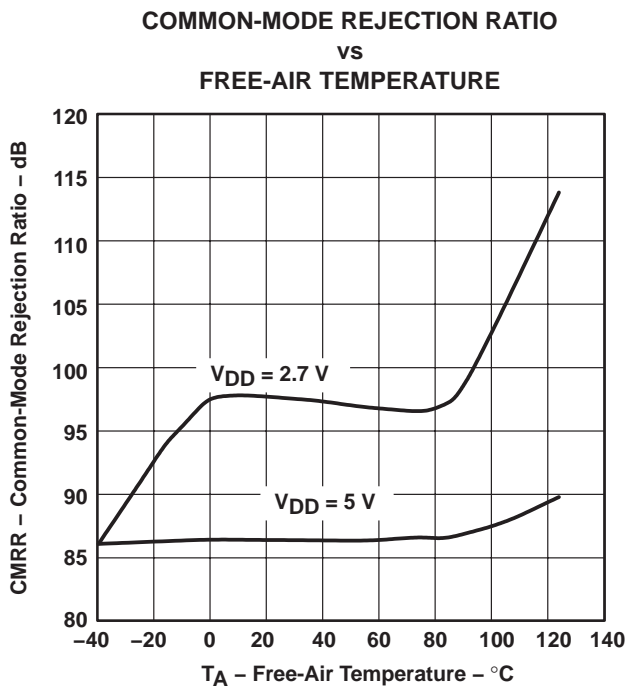


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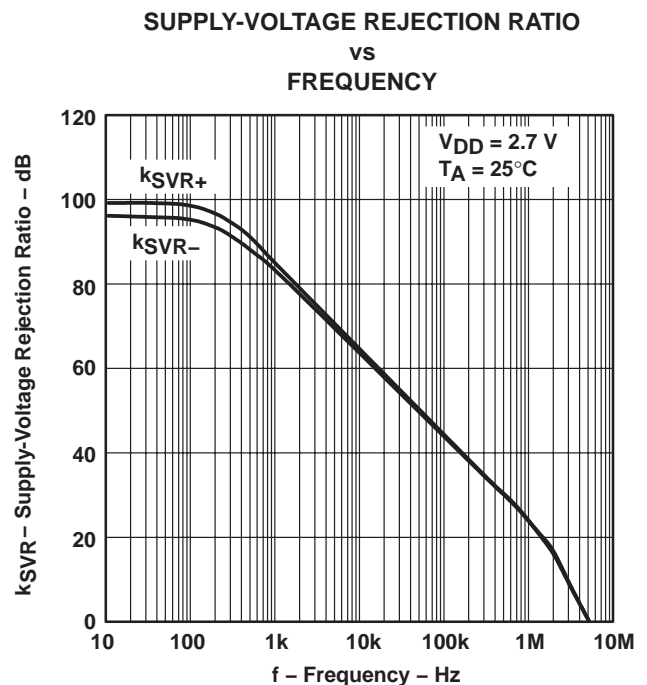


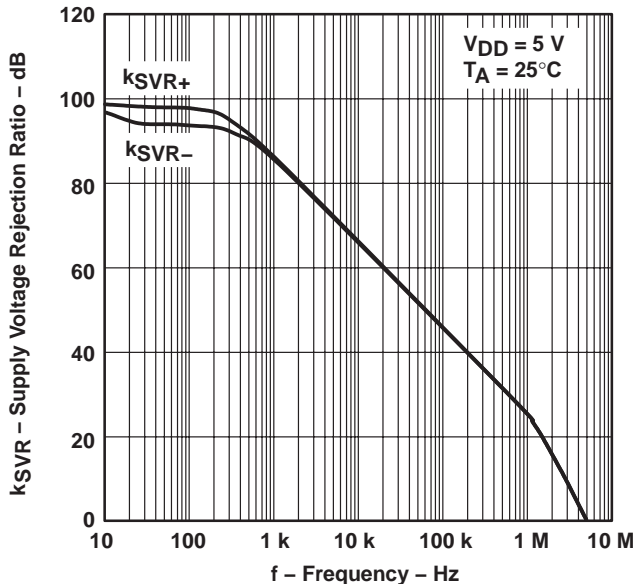
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**TLV277x-EP, TLV277xA-EP**  
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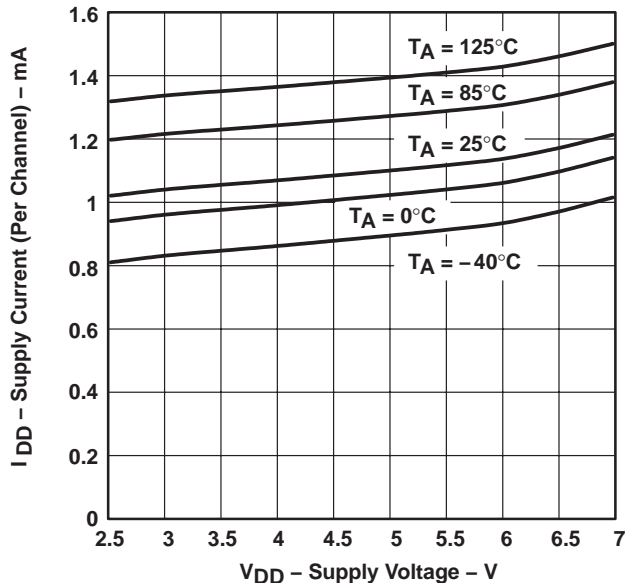
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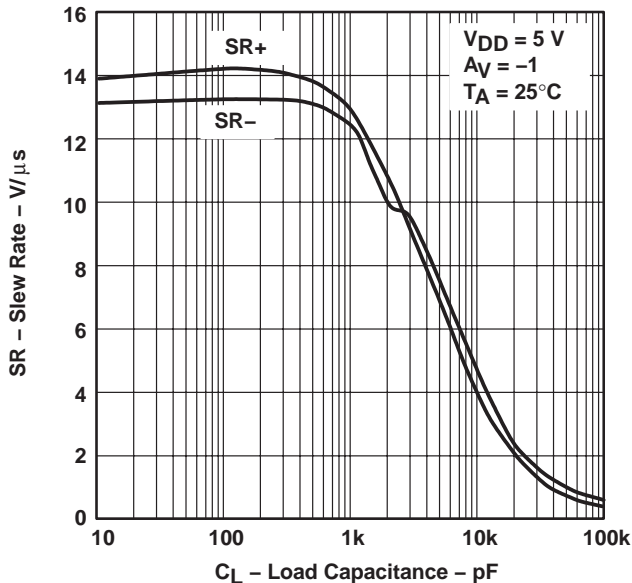
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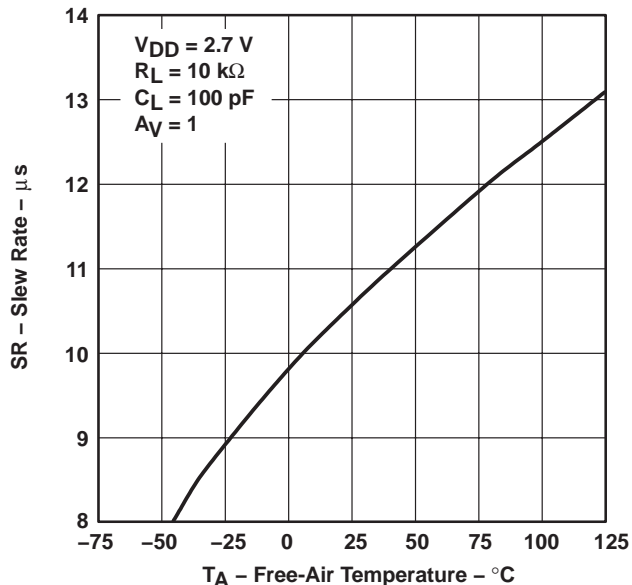
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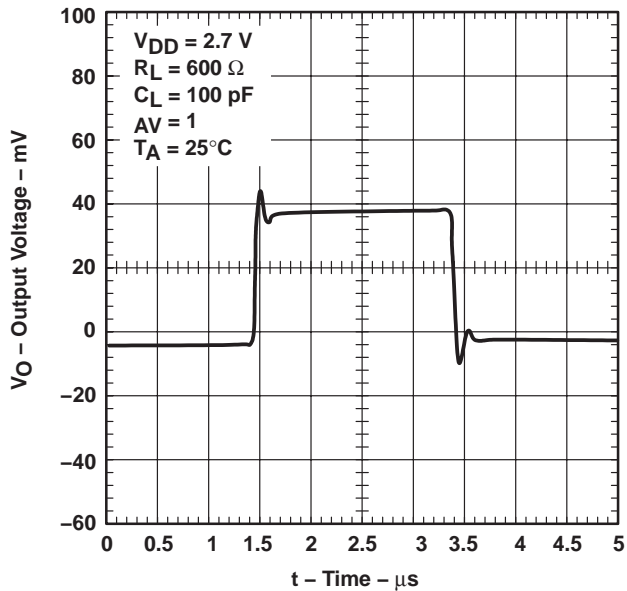


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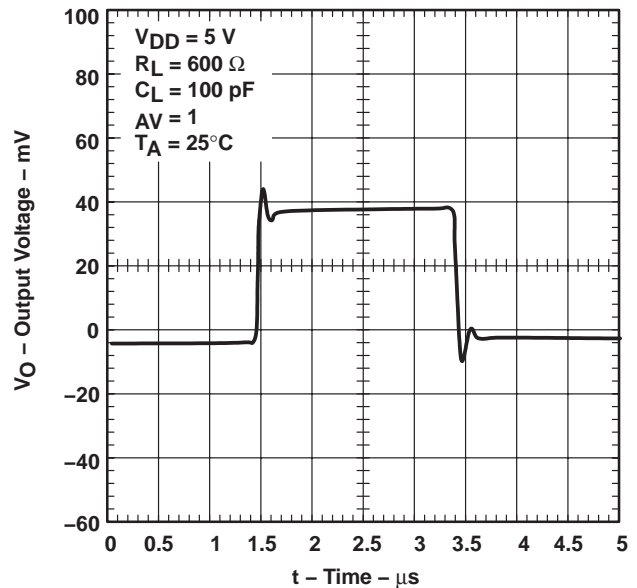
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**VOLTAGE-FOLLOWER  
SMALL-SIGNAL PULSE RESPONSE**



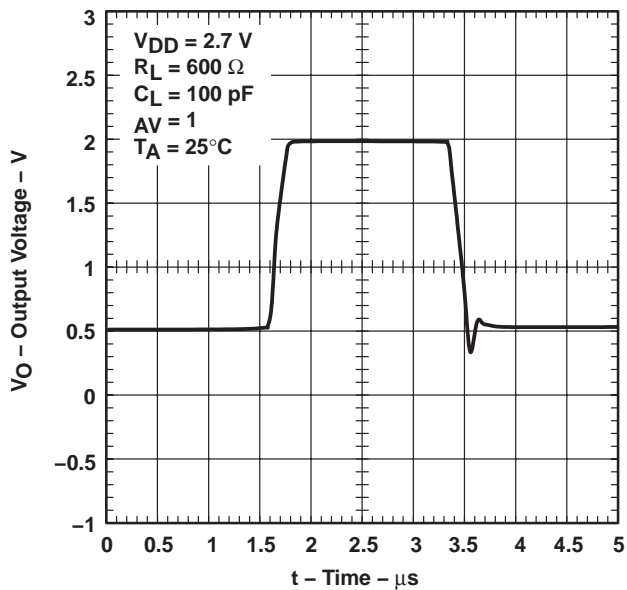
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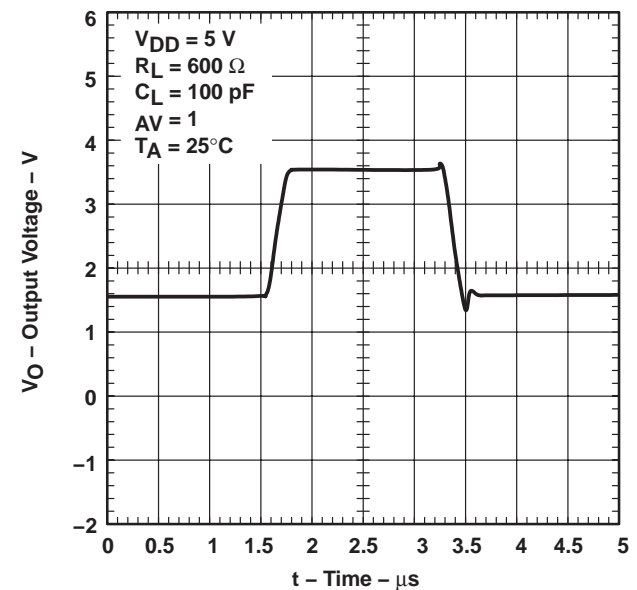
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**VOLTAGE-FOLLOWER  
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**Figure 34**

**VOLTAGE-FOLLOWER  
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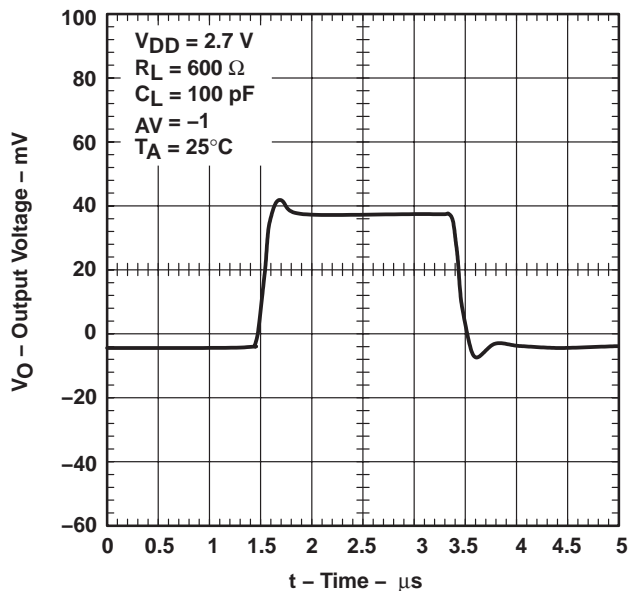
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**TLV277x-EP, TLV277xA-EP**  
**FAMILY OF 2.7-V HIGH-SLEW-RATE RAIL-TO-RAIL OUTPUT**  
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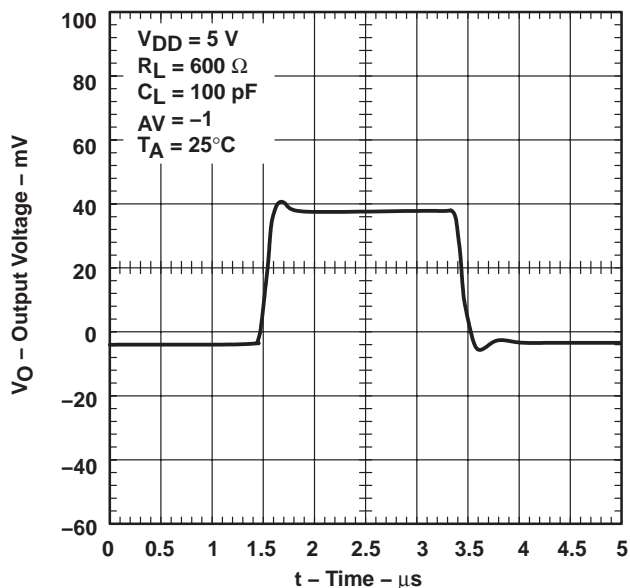
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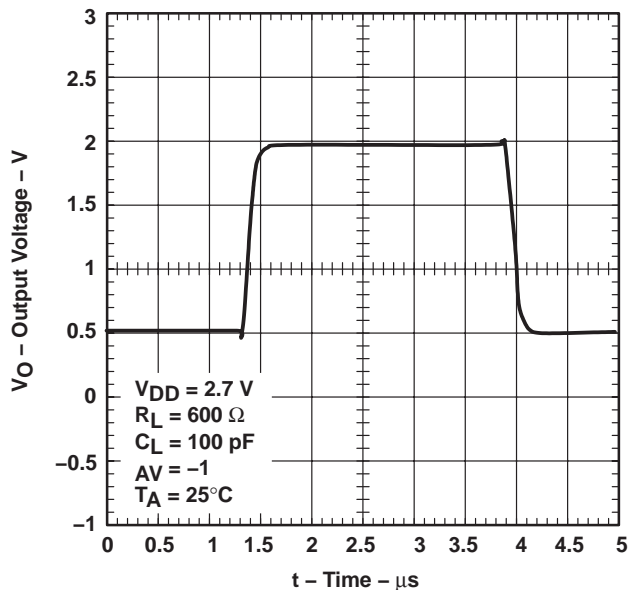
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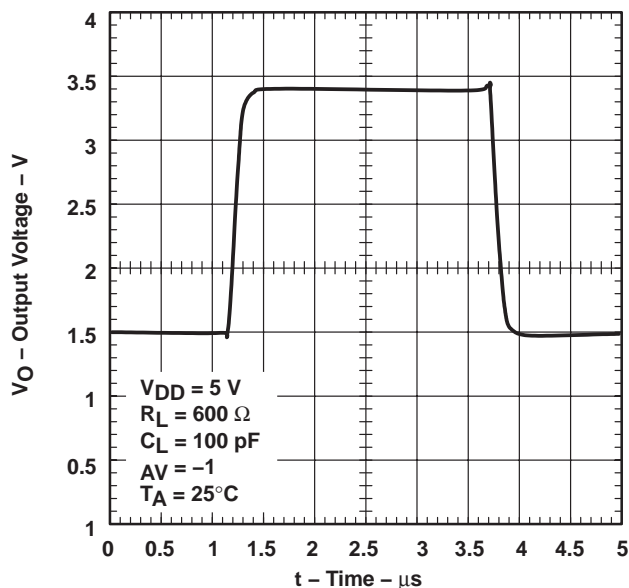
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**Figure 38**

**INVERTING LARGE-SIGNAL PULSE RESPONSE**



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TYPICAL CHARACTERISTICS

EQUIVALENT INPUT NOISE VOLTAGE  
 vs  
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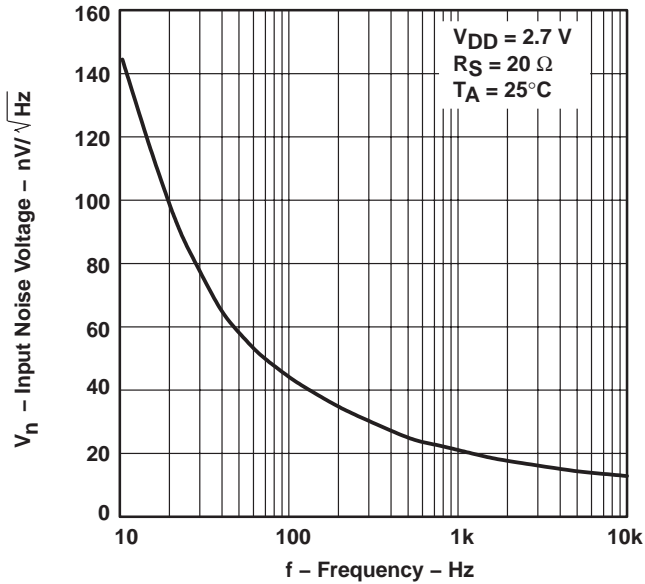


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EQUIVALENT INPUT NOISE VOLTAGE  
 vs  
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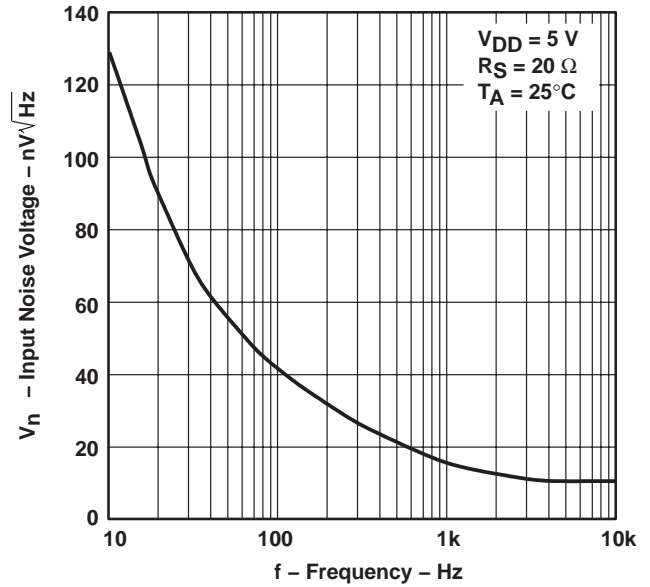


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NOISE VOLTAGE  
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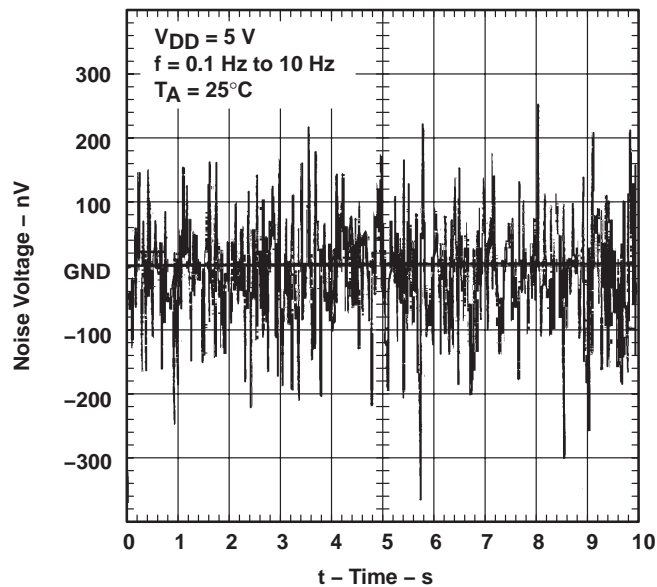


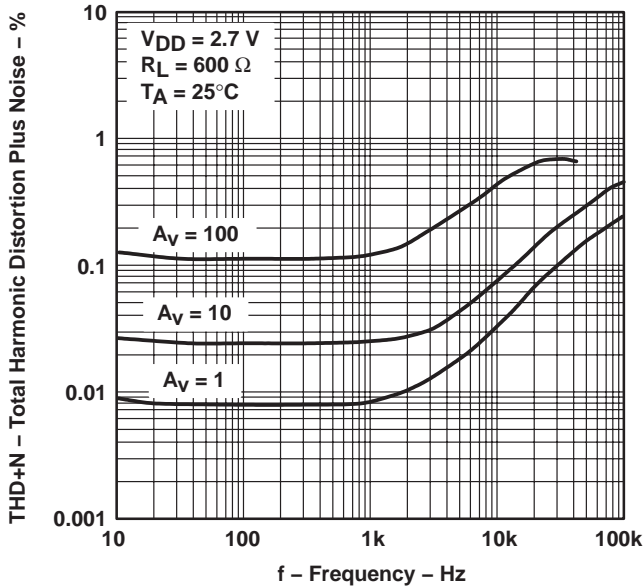
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**TLV277x-EP, TLV277xA-EP**  
**FAMILY OF 2.7-V HIGH-SLEW-RATE RAIL-TO-RAIL OUTPUT**  
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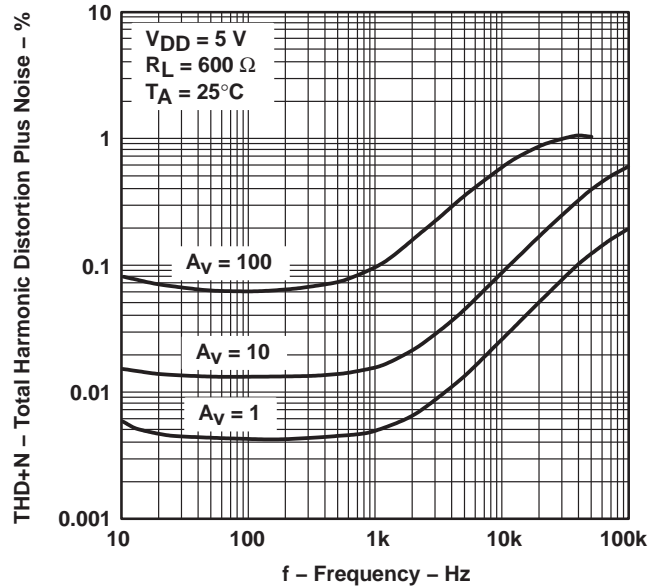
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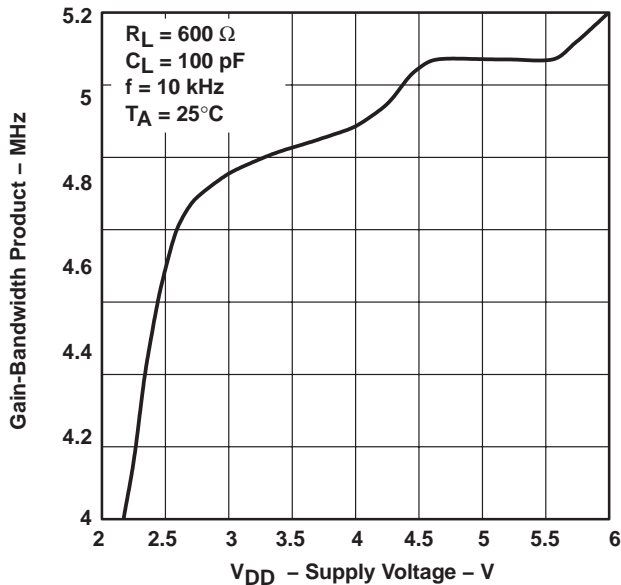
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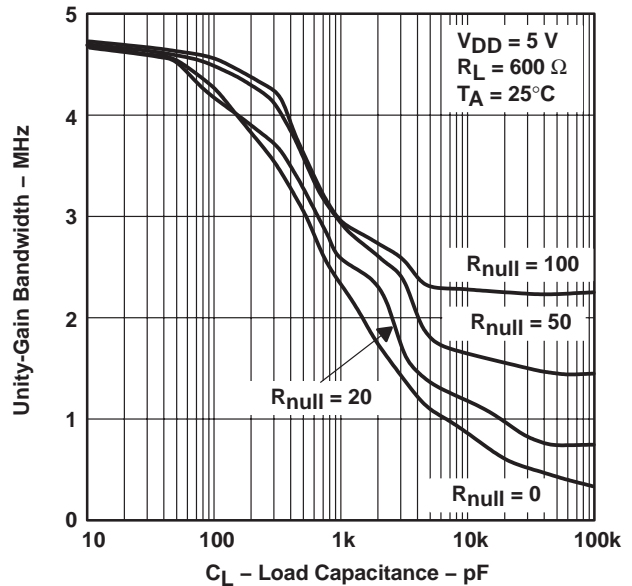
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**Figure 45**

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**Figure 46**



**TLV277x-EP, TLV277xA-EP**  
**FAMILY OF 2.7-V HIGH-SLEW-RATE RAIL-TO-RAIL OUTPUT**  
**OPERATIONAL AMPLIFIERS WITH SHUTDOWN**

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**TYPICAL CHARACTERISTICS**

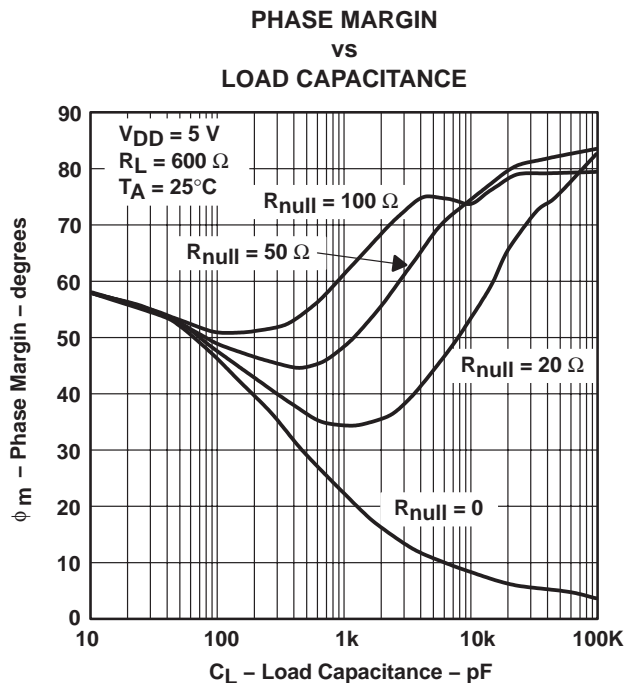


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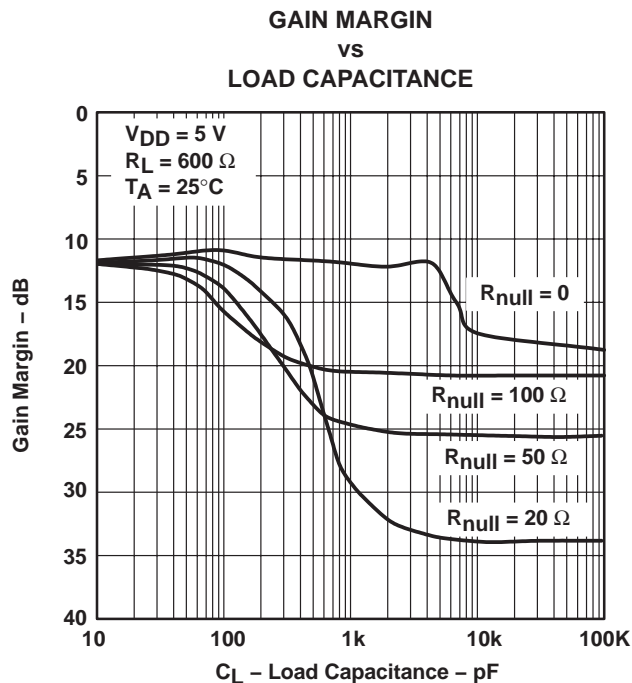


Figure 48

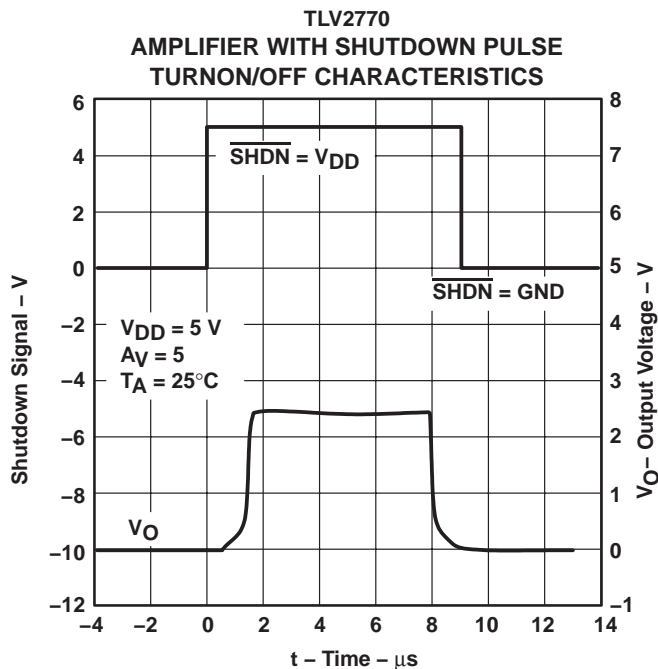


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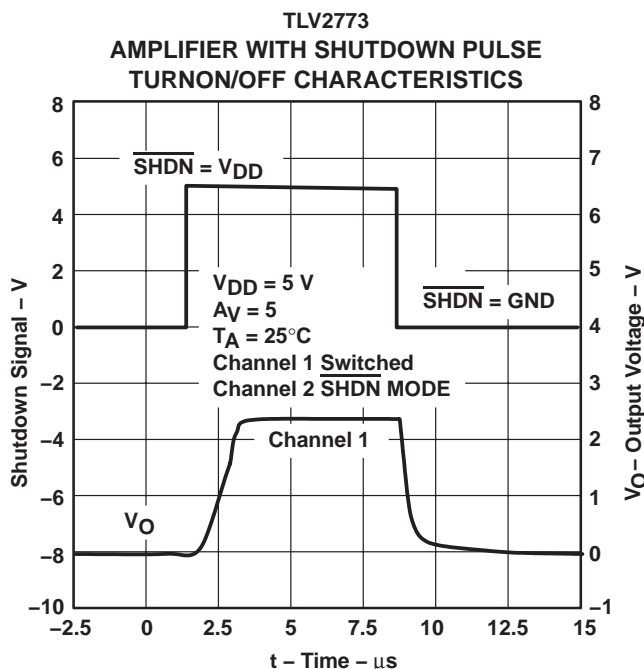
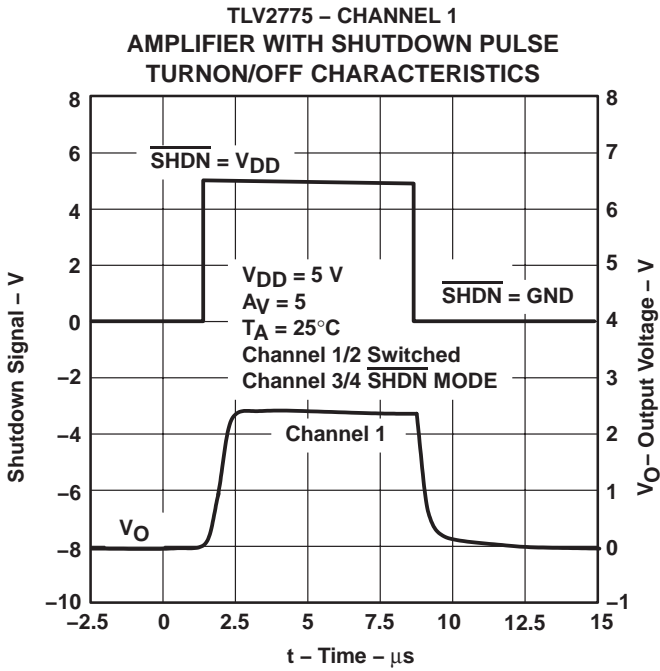


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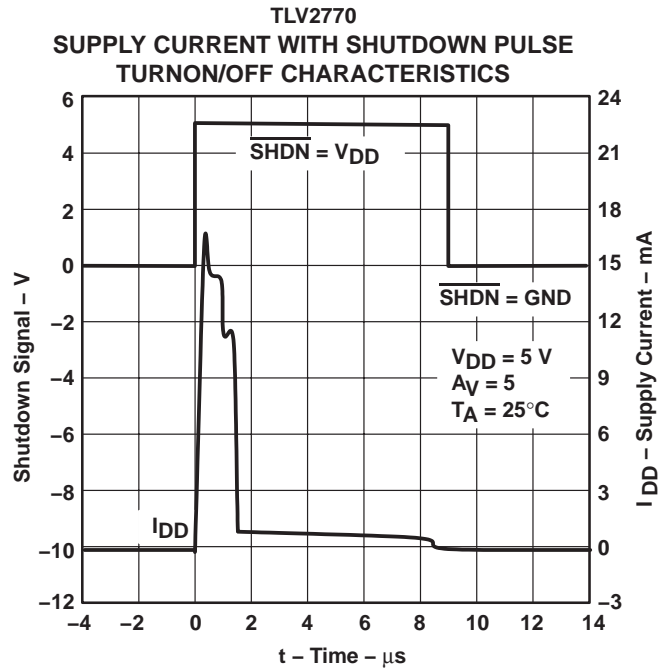
**TLV277x-EP, TLV277xA-EP**  
**FAMILY OF 2.7-V HIGH-SLEW-RATE RAIL-TO-RAIL OUTPUT**  
**OPERATIONAL AMPLIFIERS WITH SHUTDOWN**

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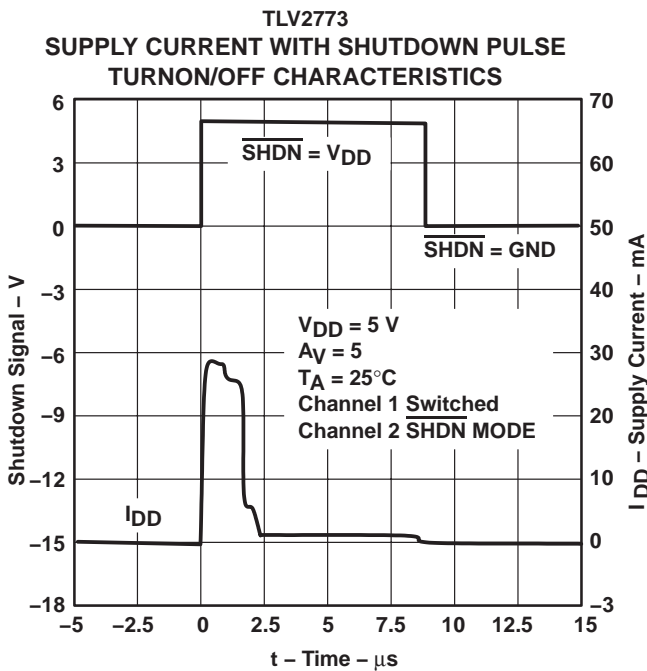
**TYPICAL CHARACTERISTICS**



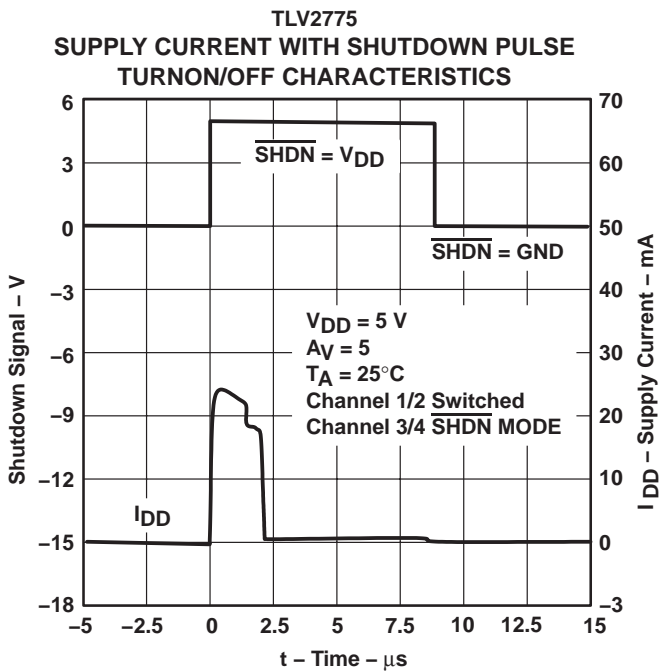
**Figure 51**



**Figure 52**



**Figure 53**



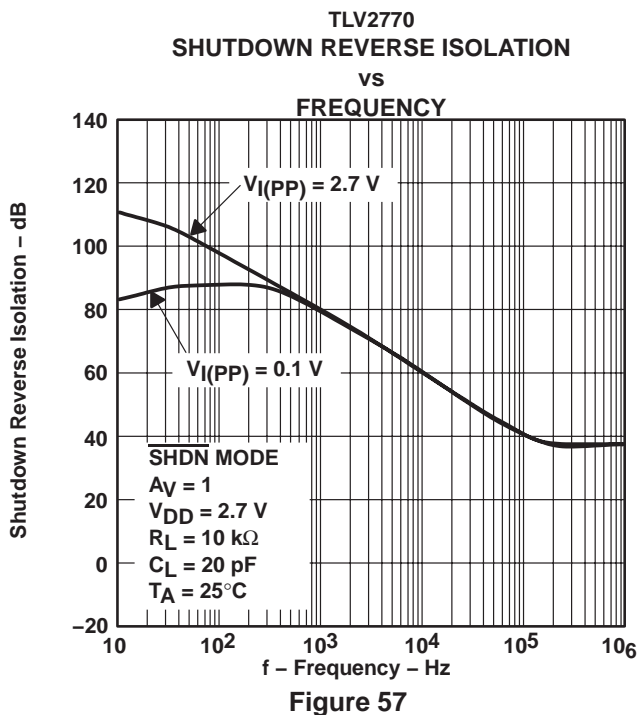
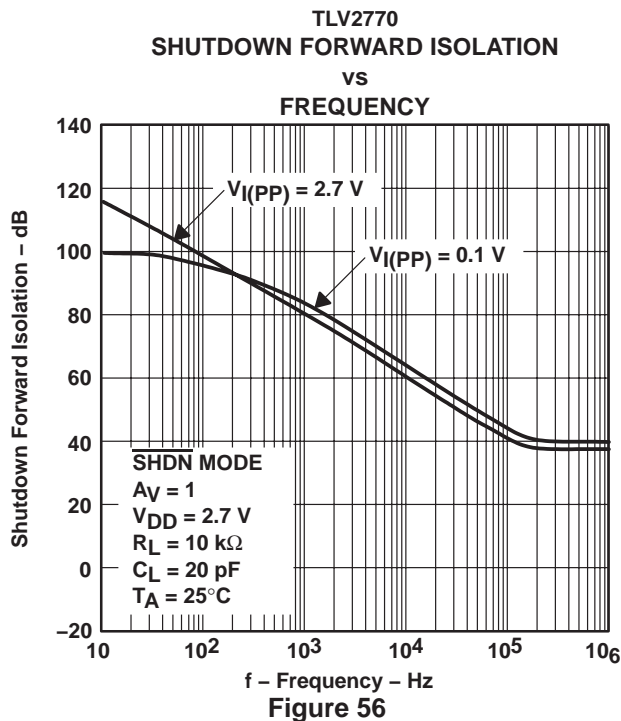
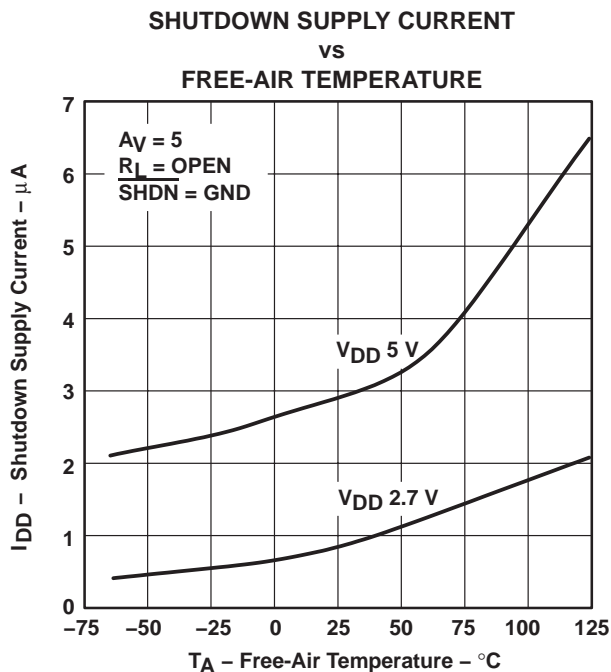
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**TLV277x-EP, TLV277xA-EP**  
**FAMILY OF 2.7-V HIGH-SLEW-RATE RAIL-TO-RAIL OUTPUT**  
**OPERATIONAL AMPLIFIERS WITH SHUTDOWN**

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**TYPICAL CHARACTERISTICS**



# TLV277x-EP, TLV277xA-EP FAMILY OF 2.7-V HIGH-SLEW-RATE RAIL-TO-RAIL OUTPUT OPERATIONAL AMPLIFIERS WITH SHUTDOWN

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## PARAMETER MEASUREMENT INFORMATION

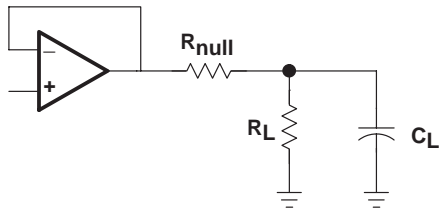


Figure 58

### driving a capacitive load

When the amplifier is configured in this manner, capacitive loading directly on the output will decrease the device's phase margin leading to high frequency ringing or oscillations. Therefore, for capacitive loads of greater than 10 pF, it is recommended that a resistor be placed in series ( $R_{NULL}$ ) with the output of the amplifier (See Figure 59). A minimum value of 20  $\Omega$  should work well for most applications.

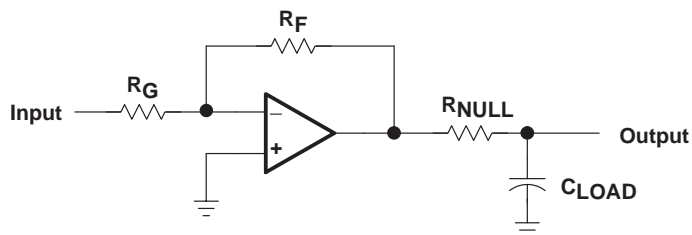
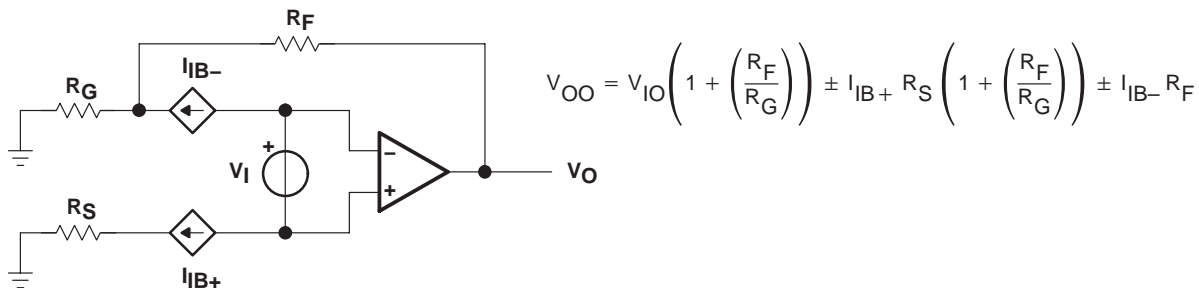


Figure 59. Driving a Capacitive Load

## APPLICATION INFORMATION

### offset voltage

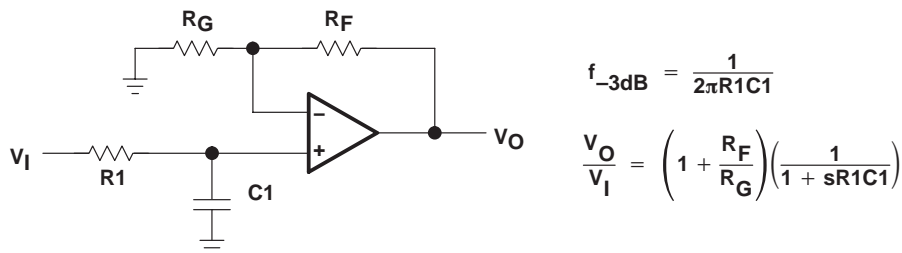
The output offset voltage, ( $V_{OO}$ ) is the sum of the input offset voltage ( $V_{IO}$ ) and both input bias currents ( $I_{IB}$ ) times the corresponding gains. The following schematic and formula can be used to calculate the output offset voltage:



**Figure 60. Output Offset Voltage Model**

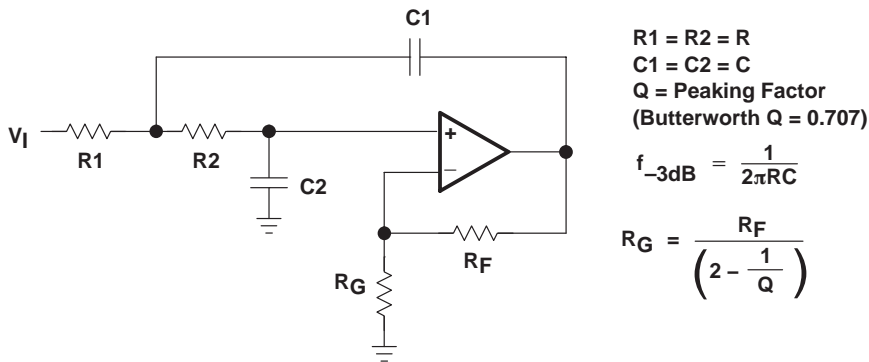
### general configurations

When receiving low-level signals, limiting the bandwidth of the incoming signals into the system is often required. The simplest way to accomplish this is to place an RC filter at the noninverting terminal of the amplifier (see Figure 61).



**Figure 61. Single-Pole Low-Pass Filter**

If even more attenuation is needed, a multiple pole filter is required. The Sallen-Key filter can be used for this task. For best results, the amplifier should have a bandwidth that is eight to ten times the filter frequency bandwidth. Failure to do this can result in phase shift of the amplifier.



**Figure 62. Two Pole Low Pass Sallen Key Filter**

# TLV277x-EP, TLV277xA-EP FAMILY OF 2.7-V HIGH-SLEW-RATE RAIL-TO-RAIL OUTPUT OPERATIONAL AMPLIFIERS WITH SHUTDOWN

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## APPLICATION INFORMATION

### using the TLV2772 as an accelerometer interface

The schematic (see Figure 63) shows the ACH04-08-05 interfaced to the TLV1544 10-bit analog-to-digital converter (ADC).

The ACH04-08-05 is a shock sensor designed to convert mechanical acceleration into electrical signals. The sensor contains three piezoelectric sensing elements oriented to simultaneously measure acceleration in three orthogonal, linear axes (x, y, z). The operating frequency is 0.5 Hz to 5 kHz. The output is buffered with an internal JFET and has a typical output voltage of 1.80 mV/g for the x and y axis and 1.35 mV/g for the z axis.

Amplification and frequency shaping of the shock sensor output is done by the TLV2772 rail-to-rail operational amplifier. The TLV2772 is ideal for this application as it offers high input impedance, good slew rate, and excellent dc precision. The rail-to-rail output swing and high output drive are perfect for driving the analog input of the TLV1544 ADC.

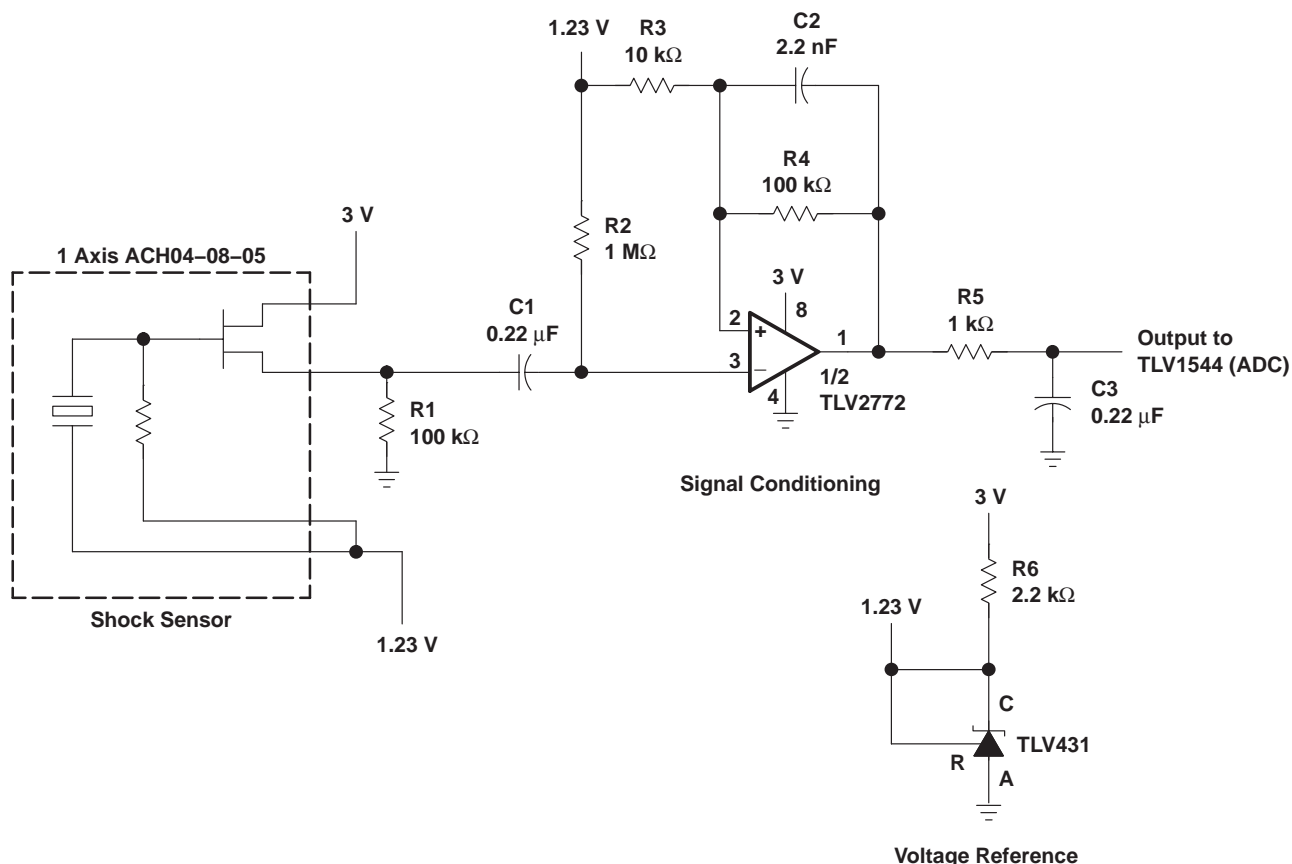


Figure 63. Accelerometer Interface Schematic

The sensor signal must be amplified and frequency-shaped to provide a signal the ADC can properly convert into the digital domain. Figure 63 shows the topology used in this application for one axis of the sensor. This system is powered from a single 3-V supply. Configuring the TLV431 with a 2.2-kΩ resistor produces a reference voltage of 1.23 V. This voltage is used to bias the operational amplifier and the internal JFETs in the shock sensor.

## APPLICATION INFORMATION

### gain calculation

Since the TLV2772 is capable of rail-to-rail output using a 3-V supply,  $V_O = 0$  (min) to 3 V (max). With no signal from the sensor, nominal  $V_O =$  reference voltage = 1.23 V. Therefore, the maximum negative swing from nominal is  $0\text{ V} - 1.23\text{ V} = -1.23\text{ V}$  and the maximum positive swing is  $3\text{ V} - 1.23\text{ V} = 1.77\text{ V}$ . By modeling the shock sensor as a low impedance voltage source with output of 2.25 mV/g (max) in the x and y axis and 1.70 mV/g (max) in the z axis, the gain of the circuit is calculated by equation 1.

$$\text{Gain} = \frac{\text{Output Swing}}{\text{Sensor Signal} \times \text{Acceleration}} \quad (1)$$

To avoid saturation of the operational amplifier, the gain calculations are based on the maximum negative swing of  $-1.23\text{ V}$  and the maximum sensor output of 2.25 mV/g (x and y axis) and 1.70 mV/g (z axis).

$$\text{Gain (x, y)} = \frac{-1.23\text{ V}}{2.25\text{ mV/g} \times -50\text{ g}} = 10.9 \quad (2)$$

and

$$\text{Gain (z)} = \frac{-1.23\text{ V}}{1.70\text{ mV/g} \times -50\text{ g}} = 14.5 \quad (3)$$

By selecting  $R_3 = 10\text{ k}\Omega$  and  $R_4 = 100\text{ k}\Omega$ , in the x and y channels, a gain of 11 is realized. By selecting  $R_3 = 7.5\text{ k}\Omega$  and  $R_4 = 100\text{ k}\Omega$ , in the z channel, a gain of 14.3 is realized. The schematic shows the configuration for either the x or y axis.

### bandwidth calculation

To calculate the component values for the frequency shaping characteristics of the signal conditioning circuit, 1 Hz and 500 Hz are selected as the minimum required 3-dB bandwidth.

To minimize the value of the input capacitor (C1) required to set the lower cutoff frequency requires a large value resistor for R2. A 1-M $\Omega$  resistor is used in this example. To set the lower cutoff frequency, the required capacitor value for C1 is:

$$C1 = \frac{1}{2\pi f_{\text{LOW}} R_2} = 0.159\text{ }\mu\text{F} \quad (4)$$

Using a value of 0.22  $\mu\text{F}$ , a more common value of capacitor, the lower cutoff frequency is 0.724 Hz.

To minimize the phase shift in the feedback loop caused by the input capacitance of the TLV2772, it is best to minimize the value of the feedback resistor R4. However, to reduce the required capacitance in the feedback loop a large value for R4 is required. Therefore, a compromise for the value of R4 must be made. In this circuit, a value of 100 k $\Omega$  has been selected. To set the upper cutoff frequency, the required capacitor value for C2 is:

$$C2 = \frac{1}{2\pi f_{\text{HIGH}} R_4} = 3.18\text{ }\mu\text{F} \quad (5)$$

Using a 2.2-nF capacitor, the upper cutoff frequency is 724 Hz.

R5 and C3 also cause the signal response to roll off. Therefore, it is beneficial to design this roll-off point to begin at the upper cutoff frequency. Assuming a value of 1 k $\Omega$  for R5, the value for C3 is calculated to be 0.22  $\mu\text{F}$ .

# TLV277x-EP, TLV277xA-EP FAMILY OF 2.7-V HIGH-SLEW-RATE RAIL-TO-RAIL OUTPUT OPERATIONAL AMPLIFIERS WITH SHUTDOWN

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## APPLICATION INFORMATION

### circuit layout considerations

To achieve the levels of high performance of the TLV277x, follow proper printed-circuit board design techniques. A general set of guidelines is given in the following.

- Ground planes—It is highly recommended that a ground plane be used on the board to provide all components with a low inductive ground connection. However, in the areas of the amplifier inputs and output, the ground plane can be removed to minimize the stray capacitance.
- Proper power supply decoupling—Use a 6.8- $\mu$ F tantalum capacitor in parallel with a 0.1- $\mu$ F ceramic capacitor on each supply terminal. It may be possible to share the tantalum among several amplifiers depending on the application, but a 0.1- $\mu$ F ceramic capacitor should always be used on the supply terminal of every amplifier. In addition, the 0.1- $\mu$ F capacitor should be placed as close as possible to the supply terminal. As this distance increases, the inductance in the connecting trace makes the capacitor less effective. The designer should strive for distances of less than 0.1 inches between the device power terminals and the ceramic capacitors.
- Sockets—Sockets can be used but are not recommended. The additional lead inductance in the socket pins will often lead to stability problems. Surface-mount packages soldered directly to the printed-circuit board is the best implementation.
- Short trace runs/compact part placements—Optimum high performance is achieved when stray series inductance has been minimized. To realize this, the circuit layout should be made as compact as possible, thereby minimizing the length of all trace runs. Particular attention should be paid to the inverting input of the amplifier. Its length should be kept as short as possible. This minimizes stray capacitance at the input of the amplifier.
- Surface-mount passive components—Using surface-mount passive components is recommended for high performance amplifier circuits for several reasons. First, because of the extremely low lead inductance of surface-mount components, the problem with stray series inductance is greatly reduced. Second, the small size of surface-mount components naturally leads to a more compact layout thereby minimizing both stray inductance and capacitance. If leaded components are used, it is recommended that the lead lengths be kept as short as possible.

### APPLICATION INFORMATION

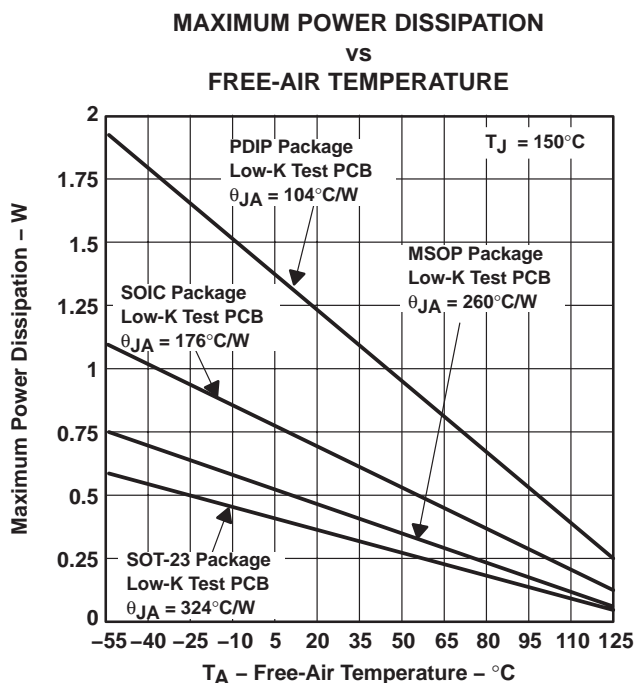
#### general power dissipation considerations

For a given  $\theta_{JA}$ , the maximum power dissipation is shown in Figure 64 and is calculated by the following formula:

$$P_D = \left( \frac{T_{MAX} - T_A}{\theta_{JA}} \right)$$

Where:

- $P_D$  = Maximum power dissipation of TLV277x IC (watts)
- $T_{MAX}$  = Absolute maximum junction temperature (150°C)
- $T_A$  = Free-ambient air temperature (°C)
- $\theta_{JA}$  =  $\theta_{JC} + \theta_{CA}$
- $\theta_{JC}$  = Thermal coefficient from junction to case
- $\theta_{CA}$  = Thermal coefficient from case to ambient air (°C/W)



NOTE A: Results are with no air flow and using JEDEC Standard Low-K test PCB.

**Figure 64. Maximum Power Dissipation vs Free-Air Temperature**

# TLV277x-EP, TLV277xA-EP FAMILY OF 2.7-V HIGH-SLEW-RATE RAIL-TO-RAIL OUTPUT OPERATIONAL AMPLIFIERS WITH SHUTDOWN

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## APPLICATION INFORMATION

### shutdown function

Three members of the TLV277x family (TLV2770/3/5) have a shutdown terminal for conserving battery life in portable applications. When the shutdown terminal is tied low, the supply current is reduced to  $0.8 \mu\text{A}/\text{channel}$ , the amplifier is disabled, and the outputs are placed in a high impedance mode. To enable the amplifier, the shutdown terminal can either be left floating or pulled high. When the shutdown terminal is left floating, care must be taken to ensure that parasitic leakage current at the shutdown terminal does not inadvertently place the operational amplifier into shutdown. The shutdown terminal threshold is always referenced to  $V_{DD}/2$ . Therefore, when operating the device with split supply voltages (e.g.  $\pm 2.5 \text{ V}$ ), the shutdown terminal must be pulled to  $V_{DD-}$  (not GND) to disable the operational amplifier.

The amplifier output with a shutdown pulse is shown in Figures 48, 49, and 50. The amplifier is powered with a single 5-V supply and configured as a noninverting configuration with a gain of 5. The amplifier turnon and turnoff times are measured from the 50% point of the shutdown pulse to the 50% point of the output waveform. The times for the single, dual, and quad are listed in the data tables. The bump on the rising edge of the TLV2770 output waveform is due to the start-up circuit on the bias generator. For the dual and quad (TLV2773/5), this bump is attributed to the bias generator's start-up circuit as well as the crosstalk between the other channel(s), which are in shutdown.

Figures 55 and 56 show the amplifier's forward and reverse isolation in shutdown. The operational amplifier is powered by  $\pm 1.35\text{-V}$  supplies and configured as a voltage follower ( $A_V = 1$ ). The isolation performance is plotted across frequency for both  $0.1 V_{PP}$  and  $2.7 V_{PP}$  input signals. During normal operation, the amplifier would not be able to handle a  $2.7\text{-V}_{PP}$  input signal with a supply voltage of  $\pm 1.35 \text{ V}$  since it exceeds the common-mode input voltage range ( $V_{ICR}$ ). However, this curve illustrates that the amplifier remains in shutdown even under a worst case scenario.



# TLV277x-EP, TLV277xA-EP FAMILY OF 2.7-V HIGH-SLEW-RATE RAIL-TO-RAIL OUTPUT OPERATIONAL AMPLIFIERS WITH SHUTDOWN

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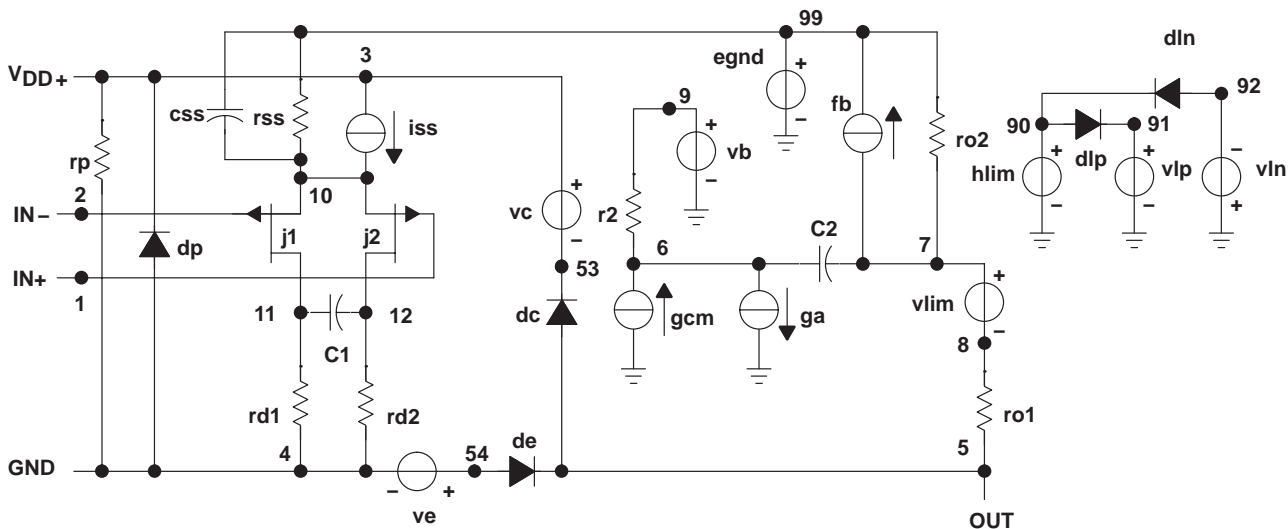
## APPLICATION INFORMATION

### macromodel information

Macromodel information provided was derived using Microsim *Parts*™ Release 8, the model generation software used with Microsim *PSpice*™. The Boyle macromodel (see Note 5) and subcircuit in Figure 65 are generated using the TLV2772 typical electrical and operating characteristics at  $T_A = 25^\circ\text{C}$ . Using this information, output simulations of the following key parameters can be generated to a tolerance of 20% (in most cases):

- Maximum positive output voltage swing
- Maximum negative output voltage swing
- Slew rate
- Quiescent power dissipation
- Input bias current
- Open-loop voltage amplification
- Unity-gain frequency
- Common-mode rejection ratio
- Phase margin
- DC output resistance
- AC output resistance
- Short-circuit output current limit

NOTE 5: G. R. Boyle, B. M. Cohn, D. O. Pederson, and J. E. Solomon, "Macromodeling of Integrated Circuit Operational Amplifiers", *IEEE Journal of Solid-State Circuits*, SC-9, 353 (1974).



\* TLV2772 operational amplifier macromodel subcircuit  
\* created using Parts release 8.0 on 12/12/97 at 10:08  
\* Parts is a MicroSim product.

\* connections: noninverting input  
\* |  
\* | inverting input  
\* | | positive power supply  
\* | | | negative power supply  
\* | | | | output  
\* | | | | |

.subckt TLV2772

	1	2	3	4	5
c1	11	12	2.8868E-12		
c2	6	7	10.000E-12		
css	10	99	2.6302E-12		
dc	5	53	dc	.82001	
de	54	5	dc	.82001	
dln	92	90	dx		
dlp	90	91	dx		
dp	4	3	dx		
egnd	99	0	poly(2) (3,0) (4,0) 0 .5 .5		
fb	7	99	poly(5) vb vc ve vlp vln 0		
ga	6	0	15.513E6 -1E3 1E3 16E6 -16E6		
gcm	0	6	10 99 9.4472E-9		

iss	3	10	dc	145.50E-6
hlim	90	0	vlim	1K
j1	11	2	10	jx1
j2	12	1	10	jx2
r2	6	9	100.00E3	
rd1	4	11	5.3052E3	
rd2	4	12	5.3052E3	
ro1	8	5	17.140	
ro2	7	99	17.140	
rp	3	4	4.5455E3	
rss	10	99	1.3746E6	
vb	9	0	dc	0
vc	3	53	dc	.82001
ve	54	4	dc	.82001
vlim	7	8	dc	0
vlp	91	0	dc	47
vln	0	92	dc	47
.model dx			D(Is=800.00E-18)	
.model dy			D(Is=800.00E-18 Rs=1m Cjo=10p)	
.model jx1			PJF(Is=2.2500E-12 Beta=244.20E-6 + Vto=-.99765)	
.model jx2			PJF(Is=1.7500E-12 Beta=244.20E-6 + Vto=-1.002350)	
.ends				

\*\$

Figure 65. Boyle Macromodel and Subcircuit

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**PACKAGING INFORMATION**

Orderable Device	Status <sup>(1)</sup>	Package Type	Package Drawing	Pins	Package Qty	Eco Plan <sup>(2)</sup>	Lead/Ball Finish	MSL Peak Temp <sup>(3)</sup>
TLV2772AMDREP	ACTIVE	SOIC	D	8	2500	Green (RoHS & no Sb/Br)	CU NIPDAU	Level-1-260C-UNLIM
TLV2774AMDREP	ACTIVE	SOIC	D	14	2500	Green (RoHS & no Sb/Br)	CU NIPDAU	Level-1-260C-UNLIM
TLV2774MDREP	ACTIVE	SOIC	D	14	2500	Green (RoHS & no Sb/Br)	CU NIPDAU	Level-1-260C-UNLIM
V62/06607-02XE	ACTIVE	SOIC	D	8	2500	Green (RoHS & no Sb/Br)	CU NIPDAU	Level-1-260C-UNLIM
V62/06607-03YE	ACTIVE	SOIC	D	14	2500	Green (RoHS & no Sb/Br)	CU NIPDAU	Level-1-260C-UNLIM
V62/06607-04YE	ACTIVE	SOIC	D	14	2500	Green (RoHS & no Sb/Br)	CU NIPDAU	Level-1-260C-UNLIM

<sup>(1)</sup> The marketing status values are defined as follows:

**ACTIVE:** Product device recommended for new designs.

**LIFEBUY:** TI has announced that the device will be discontinued, and a lifetime-buy period is in effect.

**NRND:** Not recommended for new designs. Device is in production to support existing customers, but TI does not recommend using this part in a new design.

**PREVIEW:** Device has been announced but is not in production. Samples may or may not be available.

**OBSOLETE:** TI has discontinued the production of the device.

<sup>(2)</sup> Eco Plan - The planned eco-friendly classification: Pb-Free (RoHS), Pb-Free (RoHS Exempt), or Green (RoHS & no Sb/Br) - please check <http://www.ti.com/productcontent> for the latest availability information and additional product content details.

**TBD:** The Pb-Free/Green conversion plan has not been defined.

**Pb-Free (RoHS):** TI's terms "Lead-Free" or "Pb-Free" mean semiconductor products that are compatible with the current RoHS requirements for all 6 substances, including the requirement that lead not exceed 0.1% by weight in homogeneous materials. Where designed to be soldered at high temperatures, TI Pb-Free products are suitable for use in specified lead-free processes.

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**Green (RoHS & no Sb/Br):** TI defines "Green" to mean Pb-Free (RoHS compatible), and free of Bromine (Br) and Antimony (Sb) based flame retardants (Br or Sb do not exceed 0.1% by weight in homogeneous material)

<sup>(3)</sup> MSL, Peak Temp. -- The Moisture Sensitivity Level rating according to the JEDEC industry standard classifications, and peak solder temperature.

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**OTHER QUALIFIED VERSIONS OF TLV2772A-EP, TLV2774-EP, TLV2774A-EP, TLV277X-EP, TLV277XA-EP :**

● Catalog: [TLV2772A](#), [TLV2774](#), [TLV2774A](#), [TLV277X](#), [TLV277XA](#)

● Automotive: [TLV2772A-Q1](#)

● Military: [TLV2772AM](#)

NOTE: Qualified Version Definitions:

● Catalog - TI's standard catalog product

● Automotive - Q100 devices qualified for high-reliability automotive applications targeting zero defects

● Military - QML certified for Military and Defense Applications

**TAPE AND REEL INFORMATION**



**QUADRANT ASSIGNMENTS FOR PIN 1 ORIENTATION IN TAPE**



\*All dimensions are nominal

Device	Package Type	Package Drawing	Pins	SPQ	Reel Diameter (mm)	Reel Width W1 (mm)	A0 (mm)	B0 (mm)	K0 (mm)	P1 (mm)	W (mm)	Pin1 Quadrant
TLV2772AMDREP	SOIC	D	8	2500	330.0	12.4	6.4	5.2	2.1	8.0	12.0	Q1
TLV2774AMDREP	SOIC	D	14	2500	330.0	16.4	6.5	9.0	2.1	8.0	16.0	Q1
TLV2774MDREP	SOIC	D	14	2500	330.0	16.4	6.5	9.0	2.1	8.0	16.0	Q1

**TAPE AND REEL BOX DIMENSIONS**



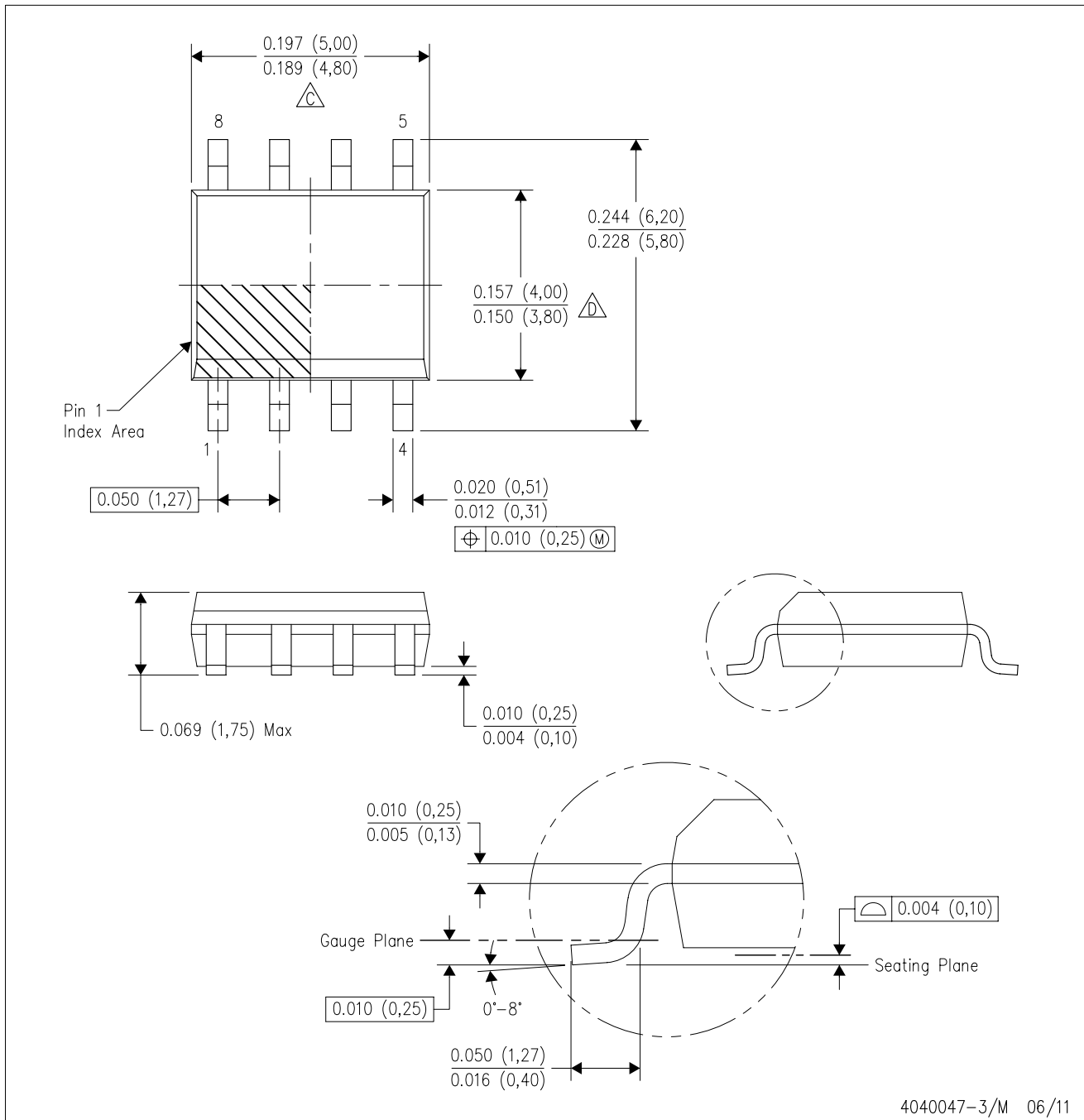
\*All dimensions are nominal

Device	Package Type	Package Drawing	Pins	SPQ	Length (mm)	Width (mm)	Height (mm)
TLV2772AMDREP	SOIC	D	8	2500	346.0	346.0	29.0
TLV2774AMDREP	SOIC	D	14	2500	333.2	345.9	28.6
TLV2774MDREP	SOIC	D	14	2500	333.2	345.9	28.6



D (R-PDSO-G8)

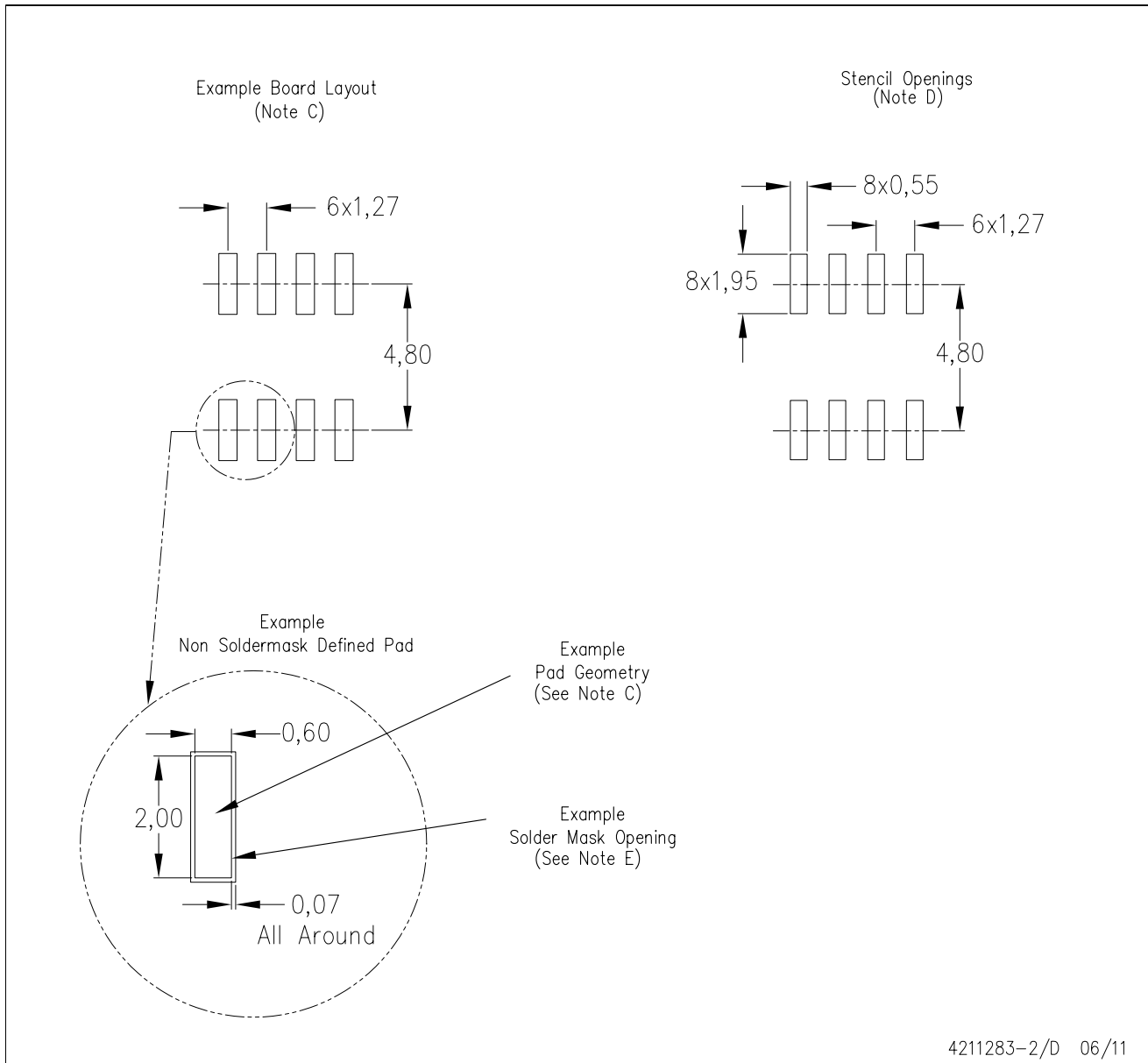
PLASTIC SMALL OUTLINE



- NOTES:
- A. All linear dimensions are in inches (millimeters).
  - B. This drawing is subject to change without notice.
  - $\triangle C$  Body length does not include mold flash, protrusions, or gate burrs. Mold flash, protrusions, or gate burrs shall not exceed 0.006 (0,15) each side.
  - $\triangle D$  Body width does not include interlead flash. Interlead flash shall not exceed 0.017 (0,43) each side.
  - E. Reference JEDEC MS-012 variation AA.

D (R-PDSO-G8)

PLASTIC SMALL OUTLINE



4211283-2/D 06/11

- NOTES:
- All linear dimensions are in millimeters.
  - This drawing is subject to change without notice.
  - Publication IPC-7351 is recommended for alternate designs.
  - Laser cutting apertures with trapezoidal walls and also rounding corners will offer better paste release. Customers should contact their board assembly site for stencil design recommendations. Refer to IPC-7525 for other stencil recommendations.
  - Customers should contact their board fabrication site for solder mask tolerances between and around signal pads.

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Data Converters	<a href="http://dataconverter.ti.com">dataconverter.ti.com</a>
DLP® Products	<a href="http://www.dlp.com">www.dlp.com</a>
DSP	<a href="http://dsp.ti.com">dsp.ti.com</a>
Clocks and Timers	<a href="http://www.ti.com/clocks">www.ti.com/clocks</a>
Interface	<a href="http://interface.ti.com">interface.ti.com</a>
Logic	<a href="http://logic.ti.com">logic.ti.com</a>
Power Mgmt	<a href="http://power.ti.com">power.ti.com</a>
Microcontrollers	<a href="http://microcontroller.ti.com">microcontroller.ti.com</a>
RFID	<a href="http://www.ti-rfid.com">www.ti-rfid.com</a>
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