LT3463/LT3463A

# Dual Micropower DC/DC Converters with Schottky Diodes 

## FGATURES

- Generates Well-Regulated Positive and Negative Outputs
- Low Quiescent Current:
$20 \mu \mathrm{~A}$ (per Converter) in Active Mode $<1 \mu \mathrm{~A}$ in Shutdown Mode
- Internal 42V Power Switches
- Internal 42V Schottky Diodes
- Low $\mathrm{V}_{\text {CESAT }}$ Switch: 180 mV at 150 mA
- Input Voltage Range: 2.4 V to 15 V
- High Output Voltages: Up to $\pm 40 \mathrm{~V}$
- Low Profile ( 0.8 mm ) $3 \mathrm{~mm} \times 3 \mathrm{~mm}$ DFN Package


## APPLICATIONS

- CCD Bias
- LCD Bias
- Handheld Computers
- Digital Cameras


## DESCRIPTIOn

The LT ${ }^{\circledR} 3463 / L T 3463$ A are dual micropower DC/DC converters with internal Schottky diodes in a 10-lead $3 \mathrm{~mm} \times$ 3 mm DFN package. Negative and positive LT3463 converters have a 250 mA current limit. The LT3463A positive converter also has a 250 mA limit, while the negative converter has a 400 mA limit. Both devices have an input voltage range of 2.4 V to 15 V , making them ideal for a wide variety of applications. Each converter features a quiescent current of only $20 \mu \mathrm{~A}$, which drops to under $1 \mu \mathrm{~A}$ in shutdown. A current limited, fixed off-time control scheme conserves operating current, resulting in high efficiency over a broad range of load current. The 42V switch enables high voltage outputs up to $\pm 40 \mathrm{~V}$ to be easily generated without the use of costly transformers. The low 300ns offtime permits the use of tiny, low profile inductors and capacitors to minimize footprint and cost in space-conscious portable applications.

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## TYPICAL APPLICATION

CCD Bias Supply (15V, -8V)


Efficiency and Power Loss


3463 TA01b

## ABSOLUTG MAXIMUM RATINGS

(Note 1)
$\mathrm{V}_{\text {IN }}, \overline{\text { SHDN1 }}, \overline{\text { SHDN2 }}$ Voltage .................................. 15V
SW1, SW2, V ${ }_{\text {OUT1 }}$ Voltage ...................................... 42V
D2 Voltage ........................................................... 42 V
FB1, FB2 Voltage Range .............................. -0.3 V to 2 V
Junction Temperature .......................................... $125^{\circ} \mathrm{C}$
Operating Ambient Temperature Range (Note 2) $\qquad$ $-40^{\circ} \mathrm{C}$ to $85^{\circ} \mathrm{C}$ Storage Temperature Range ................. $-65^{\circ} \mathrm{C}$ to $125^{\circ} \mathrm{C}$

PACKAGE/ORDER INFORMATION


Consult LTC Marketing for parts specified with wider operating temperature ranges.

ELECRACPL CMPRACTERISTICS The o denotes the specifications which apply over the full operating temperature range, otherwise specifications are at $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C} . \mathrm{V}_{I N}=2.5 \mathrm{~V}, \mathrm{~V} \overline{\mathrm{SHDN}}=2.5 \mathrm{~V}$ unless otherwise noted.

| PARAMETER | CONDITIONS |  | MIN | TYP | MAX | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Minimum Input Voltage |  |  |  | 2.2 | 2.4 | V |
| Total Quiescent Current | For Both Switchers, Not Switching |  |  | 40 | 60 | $\mu \mathrm{A}$ |
| Shutdown Current | $V_{\text {SHDN1 }}=\mathrm{V}_{\overline{\text { SHDN2 }}}=0 \mathrm{~V}$ |  |  | 0.1 | 1 | $\mu \mathrm{A}$ |
| $\mathrm{V}_{\text {REF }}$ Pin Voltage | With $124 \mathrm{k} \Omega$ to GND | $\bullet$ | 1.23 | 1.25 | 1.27 | V |
| $\mathrm{V}_{\text {REF }}$ Pin Voltage Line Regulation | With $124 \mathrm{k} \Omega$ to GND |  |  | 0.05 | 0.10 | \%/V |
| FB1 Comparator Trip Voltage | High to Low Transition | $\bullet$ | 1.225 | 1.25 | 1.275 | V |
| FB1 Comparator Hysteresis |  |  |  | 8 |  | mV |
| FB1 Line Regulation | $2.5 \mathrm{~V}<\mathrm{V}_{\text {IN }}<15 \mathrm{~V}$ |  |  | 0.05 | 0.10 | \%/V |
| FB1 Pin Bias Current (Note 3) | $\mathrm{V}_{\mathrm{FB} 1}=1.3 \mathrm{~V}$ | $\bullet$ |  | 20 | 50 | nA |
| FB2 Comparator Trip Voltage | Low to High Transition | $\bullet$ | 0 | 3 | 12 | mV |
| FB2 Comparator Hysteresis |  |  |  | 8 |  | mV |
| FB2 Line Regulation ( $\mathrm{V}_{\text {REF }}-\mathrm{V}_{\text {FB2 }}$ ) | $2.5 \mathrm{~V}<\mathrm{V}_{\text {IN }}<15 \mathrm{~V}$ |  |  | 0.05 | 0.10 | \%/V |
| FB2 Pin Bias Current (Note 4) | $\mathrm{V}_{\text {FB2 }}=-0.1 \mathrm{~V}$ | $\bullet$ |  | 20 | 50 | nA |
| SW1 Switch Off Time | $\begin{aligned} & V_{\text {OUT1 }}-V_{\text {IN }}=4 V \\ & V_{\text {OUT1 }}-V_{\text {IN }}=0 V \end{aligned}$ |  |  | $\begin{aligned} & 300 \\ & 1.5 \end{aligned}$ |  | ns $\mu \mathrm{s}$ |
| SW2 Switch Off Time | $\begin{aligned} & V_{\text {FB2 }}<0.1 \mathrm{~V} \\ & V_{\text {FB2 } 2}=1 \mathrm{~V} \end{aligned}$ |  |  | $\begin{aligned} & 300 \\ & 1.5 \end{aligned}$ |  | ns $\mu \mathrm{s}$ |
| Switch V ${ }_{\text {CESAT }}$ (SW1, SW2) | $\mathrm{I}_{\text {SW }}=150 \mathrm{~mA}$ |  |  | 180 |  | mV |
| Switch Current Limit (SW1) |  |  | 180 | 250 | 320 | mA |
| Switch Current Limit (SW2) | $\begin{aligned} & \hline \text { LT3463 } \\ & \text { LT3463A } \end{aligned}$ |  | $\begin{aligned} & 180 \\ & 320 \end{aligned}$ | $\begin{aligned} & 250 \\ & 400 \end{aligned}$ | $\begin{aligned} & 320 \\ & 460 \end{aligned}$ | $\begin{aligned} & \mathrm{mA} \\ & \mathrm{~mA} \end{aligned}$ |
| Swith Leakage Current (SW1, SW2) | Switch Off, $\mathrm{V}_{\text {SW }}=42 \mathrm{~V}$ |  |  | 0.01 | 1 | $\mu \mathrm{A}$ |
| Schottky Forward Voltage (V ${ }_{\text {OUT1 }}$, D2) | $\mathrm{I}_{\mathrm{D}}=150 \mathrm{~mA}$ |  |  | 750 |  | mV |
| Schottky Reverse Leakage Current | $\begin{aligned} & V_{\text {OUT1 } 1}-V_{S W}=42 \mathrm{~V} \\ & V_{D 2}=-42 \mathrm{~V} \end{aligned}$ |  |  | 1 | $\begin{aligned} & \hline 5 \\ & 5 \end{aligned}$ | $\mu \mathrm{A}$ $\mu \mathrm{A}$ |
| SHDN1 Pin Current | $\mathrm{V}_{\overline{\text { SHDN } 1}}=2.5 \mathrm{~V}$ |  |  | 4 | 10 | $\mu \mathrm{A}$ |
| SHDN2 Pin Current | $\mathrm{V}^{\text {SHDN2 }}=2.5 \mathrm{~V}$ |  |  | 4 | 10 | $\mu \mathrm{A}$ |
| $\overline{\text { SHDN1/SHDN2 Start-Up Threshold }}$ |  |  | 0.3 | 1 | 1.5 | V |

Note 1: Absolute Maximum Ratings are those values beyond which the life of a device may be impaired.
Note 2: The LT3463/LT3463A are guaranteed to meet performance
specifications from $0^{\circ} \mathrm{C}$ to $70^{\circ} \mathrm{C}$. Specifications over the $-40^{\circ} \mathrm{C}$ to $85^{\circ} \mathrm{C}$
operating ambient temperature range are assured by design, characterization and correlation with statistical process controls.
Note 3: Bias current flows into the FB1 pin.
Note 4: Bias current flows out of the FB2 pin.

## TYPICAL PGRFORMAOCE CHARACTERISTICS



3463 G01


3463 G04


3463 G02


3463 G05


3463 G03

## Quiescent Current



3463 G06

## PIn fUnCTIOnS

$\mathrm{V}_{\text {OUT1 }}$ (Pin 1): Output Voltage Switcher 1. This is the cathode of an internal Schottky diode whose anode is connected to the SW1 pin.
SW1 (Pin 2): Switch Pin for Switcher 1. This is the collector of the internal NPN switch. Minimize the metal trace area connected to this pin to minimize EMI.
$\mathbf{V}_{\mathbf{I N}}$ (Pin 3): Input Supply Pin. Bypass this pin with a capacitor as close to the device as possible.
SW2 (Pin 4): Switch Pin for Switcher 2. This is the collector of the internal NPN switch. Minimize the metal trace area connected to this pin to minimize EMI.

D2 (Pin 5): Diode for Switcher 2. This is the anode of an internal Schottky diode whose cathode connected to the GND pin.

FB2 (Pin 6): Feedback Pin for Switcher 2. Set the output voltage by selecting values for R3 and R4.
$V_{\text {REF }}$ (Pin 7): Voltage Reference Pin (1.25V). This pin is used along with FB 2 to set the negative output voltage for Switcher 2.
SHDN2 (Pin 8): Shutdown Pin for Switcher 2. Pull this pin above 1.5 V to enable Switcher 2. Pull below 0.3 V to turn it off. Do not leave this pin floating.

## PIn functions

SHDN1 (Pin 9): Shutdown Pin for Switcher 1. Pull this pin above 1.5 V to enable Switcher 1. Pull below 0.3 V to turn it off. Do not leave this pin floating.

GND (Pin 11): Exposed Pad. Solder this exposed pad directly to the local ground plane. This pad must be electrically connected for proper operation.

FB1 (Pin 10): Feedback Pin for Switcher 1. Set the output voltage by selecting values for R1 and R2.

## BLOCK DIAGRAM



Figure 1. Block Diagram

## OPERATION

The LT3463 uses a constant off-time control scheme to provide high efficiency over a wide range of output current. Operation can be best understood by referring to the block diagram in Figure 1. When the voltage at the FB1 pin is slightly above 1.25 V , comparator A1 disables most of the internal circuitry. Output current is then provided by capacitor C 2 , which slowly discharges until the voltage at the FB1 pin goes below the hysteresis point of A1 (typical hysteresis at the FB1 pin is 8 mV ). A1 then enables the internal circuitry, turns on power switch Q1, and the
current in inductor L1 begins ramping up. Once the switch current reaches 250 mA , comparator A2 resets the oneshot, which turns off Q1 for 300ns. Q1 turns on again and the inductor currents ramp back up to 250 mA , then A2 again resets the one-shot. This switching action continues until the output voltage is charged up (until the FB1 pin reaches 1.25 V ), then A1 turns off the internal circuitry and the cycle repeats. The second switching regulator is an inverting converter (which generates a negative output) but the basic operation is the same.

## APPLICATIONS INFORMATION

Choosing an Inductor

Several recommended inductors that work well with the LT3463 are listed in Table 1, although there are many other manufacturers and devices that can be used. Consult each manufacturer for more detailed information and for their entire selection of related parts. Many different sizes and shapes are available. Use the equations and recommendations in the next few sections to find the correct inductance value for your design.

## Table 1. Recommended Inductors

| PART | $\mathrm{L}(\mu \mathrm{H})$ | $\begin{array}{\|c\|} \hline \operatorname{MAX} \\ \mathrm{IC}(\mathrm{~mA}) \end{array}$ | $\begin{gathered} \operatorname{MAX} \\ \operatorname{DCR}(\Omega) \end{gathered}$ | $\begin{gathered} \text { HEIGHT } \\ (\mathrm{mm}) \end{gathered}$ | MANUFACTURER |
| :---: | :---: | :---: | :---: | :---: | :---: |
| CMD4D06 | $\begin{aligned} & 4.7 \\ & 10 \\ & 22 \end{aligned}$ | $\begin{aligned} & 750 \\ & 500 \\ & 310 \end{aligned}$ | $\begin{aligned} & 0.22 \\ & 0.46 \\ & 1.07 \end{aligned}$ | 0.8 | Sumida (847) 956-0666 www.sumida.com |
| CDRH3D16 | $\begin{aligned} & \hline 10 \\ & 22 \end{aligned}$ | $\begin{aligned} & 500 \\ & 310 \end{aligned}$ | $\begin{aligned} & 0.19 \\ & 0.36 \end{aligned}$ | 1.8 | Sumida |
| LP04812 | $\begin{aligned} & 4.7 \\ & 10 \\ & 22 \end{aligned}$ | $\begin{aligned} & 600 \\ & 400 \\ & 280 \end{aligned}$ | $\begin{aligned} & 0.16 \\ & 0.30 \\ & 0.64 \end{aligned}$ | 1.2 | Coilcraft (847) 639-6400 www.coilcraft.com |
| LQH32C | $\begin{aligned} & \hline 10 \\ & 15 \\ & 22 \end{aligned}$ | $\begin{aligned} & 450 \\ & 300 \\ & 250 \end{aligned}$ | $\begin{aligned} & 0.39 \\ & 0.75 \\ & 0.92 \end{aligned}$ | 1.8 | Murata (714) 852-2001 www.murata.com |
| LQH31C | 4.7 | 340 | 0.85 | 1.8 | Murata |

## Inductor Selection-Boost Regulator

The formula below calculates the appropriate inductor value to be used for a boost regulator using the LT3463 (or at least provides a good starting point). This value provides a good tradeoff in inductor size and system performance. Pick a standard inductor close to this value. A larger value can be used to slightly increase the available output current, but limit it to around twice the value calculated below, as too large of an inductance will increase the output voltage ripple without providing much additional output current. A smaller value can be used (especially for systems with output voltages greater than $12 \mathrm{~V})$ to give a smaller physical size. Inductance can be calculated as:

$$
\mathrm{L}=\frac{V_{\text {OUT }}-V_{\text {IN(MIIN })}+V_{D}}{I_{\text {LIM }}} \mathrm{t}_{\text {OFF }}
$$

where $\mathrm{V}_{\mathrm{D}}=0.5 \mathrm{~V}$ (Schottky diode voltage), $\mathrm{I}_{\text {LIM }}=250 \mathrm{~mA}$ (or 400 mA ) and $\mathrm{t}_{0 \mathrm{FF}}=300 \mathrm{~ns}$; for designs with varying $\mathrm{V}_{\text {IN }}$
such as battery powered applications, use the minimum $V_{\text {IN }}$ value in the above equation. For most regulators with output voltages below 7 V , a $4.7 \mu \mathrm{H}$ inductor is the best choice, even though the equation above might specify a smaller value.

For higher output voltages, the formula above will give large inductance values. For a 3V to 20V converter (typical LCD Bias application), a $21 \mu \mathrm{H}$ inductor is called for with the above equation, but a $10 \mu \mathrm{H}$ inductor could be used without much reduction in the maximum output current.

## Inductor Selection—Inverting Regulator

The formula below calculates the appropriate inductor value to be used for an inverting regulator using the LT3463 (or at least provides a good starting point). This value provides a good tradeoff in inductor size and system performance. Pick a standard inductor close to this value (both inductors should be the same value). A larger value can be used to slightly increase the available output current, but limit it to around twice the value calculated below, as too large of an inductance will increase the output voltage ripple without providing much additional output current. A smaller value can be used (especially for systems with output voltages greater than 12V) to give a smaller physical size. Inductance can be calculated as:

$$
\mathrm{L}=2\left(\frac{\left|\mathrm{~V}_{\text {OUT }}\right|+\mathrm{V}_{\mathrm{D}}}{\mathrm{I}_{\text {LIM }}}\right)_{\mathrm{OFF}}
$$

where $\mathrm{V}_{\mathrm{D}}=0.5 \mathrm{~V}$ (Schottky diode voltage), $\mathrm{I}_{\mathrm{LIM}}=250 \mathrm{~mA}$ (or 400 mA ) and $\mathrm{t}_{\text {off }}=300 \mathrm{~ns}$.

For higher output voltages, the formula above will give large inductance values. For a 3 V to 20 V converter (typical LCD bias application), a $49 \mu \mathrm{H}$ inductor is called for with the above equation, but a $10 \mu \mathrm{H}$ or $22 \mu \mathrm{H}$ inductor could be used without much reduction in the maximum output current.

## Inductor Selection—Inverting Charge Pump Regulator

For the inverting regulator, the voltage seen by the internal power switch is equal to the sum of the absolute value of the input and output voltages, so that generating high

## APPLICATIONS InFORMATION

output voltages from a high input voltage source will often exceed the 50V maximum switch rating. For instance, a 12 V to -40 V converter using the inverting topology would generate 52 V on the SW pin, exceeding its maximum rating. For this application, an inverting charge pump is the best topology.

The formula below calculates the approximate inductor value to be used for an inverting charge pump regulator using the LT3463. As for the boost inductor selection, a larger or smaller value can be used. For designs with varying $\mathrm{V}_{\text {IN }}$ such as battery powered applications, use the minimum $V_{\text {IN }}$ value in the equation below.

$$
L=\frac{\left|V_{\text {OUT }}\right|-V_{\text {IN }}(\text { MII })+V_{D}}{I_{\text {LIM }}} t_{\text {OFF }}
$$

## Capacitor Selection

The small size and low ESR of ceramic capacitors makes them ideal for LT3463 applications. Use only X5R and X7R types because they retain their capacitance over wider voltage and temperature ranges than other ceramic types. A $1 \mu \mathrm{~F}$ input capacitor and a $0.22 \mu \mathrm{~F}$ or $0.47 \mu \mathrm{~F}$ output capacitor are sufficient for most applications. Table 2 shows a list of several ceramic capacitor manufacturers. Consult the manufacturers for more detailed information on their entire selection of ceramic capacitors. For applications needing very low output voltage ripple, larger output capacitor values can be used.

Table 2. Recommended Ceramic Capacitor Manufacturers

| MANUFACTURER | PHONE | URL |
| :--- | :---: | :--- |
| AVX | $843-448-9411$ | www.avxcorp.com |
| Kemet | $408-986-0424$ | www.kemet.com |
| Murata | $814-237-1431$ | www.murata.com |
| Taiyo Yuden | $408-573-4150$ | www.t-yuden.com |

## Inrush Current

When $\mathrm{V}_{\text {IN }}$ is increased from ground to operating voltage while the output capacitor is discharged, an inrush current will flow through the inductor and integrated Schottky diode into the output capacitor. Conditions that increase
inrush current include a larger more abrupt voltage step at $\mathrm{V}_{\mathrm{IN}}$, a larger output capacitor tied to the outputs, and an inductor with a low saturation current.

While the internal diode is designed to handle such events, the inrush current should not be allowed to exceed 1 amp. For circuits that use output capacitor values within the recommended range and have input voltages of less than 5 V , inrush current remains low, posing no hazard to the device. In cases where there are large steps at $\mathrm{V}_{\text {IN }}$ and/or a large capacitor is used at the outputs, inrush current should be measured to ensure safe operation.

## Setting the Output Voltages

The output voltages are programmed using two feedback resistors. As shown in Figure 1, resistors R1 and R2 program the positive output voltage (for Switcher 1), and resistors R3 and R4 program the negative output voltage (for Switcher 2) according to the following formulas:

$$
\begin{aligned}
& V_{\text {OUT } 1}=1.25 \mathrm{~V}\left(1+\frac{\mathrm{R} 2}{\mathrm{R} 1}\right) \\
& \mathrm{V}_{\text {OUT } 2}=-1.25 \mathrm{~V}\left(\frac{\mathrm{R} 4}{\mathrm{R} 3}\right)
\end{aligned}
$$

R1 and R3 are typically $1 \%$ resistors with values in the range of 50 k to 250 k .

## Board Layout Considerations

As with all switching regulators, careful attention must be paid to the PCB board layout and component placement. To maximize efficiency, switch rise and fall times are made as short as possible. To prevent electromagnetic interference (EMI) problems, proper layout of the high frequency switching path is essential. The voltage signal of the SW pin has sharp rising and falling edges. Minimize the length and area of all traces connected to the SW pin and always use a ground plane under the switching regulator to minimize interplane coupling. In addition, the ground connection for the feedback resistor R1 should be tied directly to the GND pin and not shared with any other component, ensuring a clean, noise-free connection.

## TYPICAL APPLICATION

Dual Output $\pm 20 \mathrm{~V}$ Converter


## PACKAGE DESCRIPTION

DD Package
10-Lead Plastic DFN ( $3 \mathrm{~mm} \times 3 \mathrm{~mm}$ )


RECOMMENDED SOLDER PAD PITCH AND DIMENSIONS

NOTE:

1. DRAWING TO BE MADE A JEDEC PACKAGE OUTLINE MO-229 VARIATION OF (WEED-2). CHECK THE LTC WEBSITE DATA SHEET FOR CURRENT STATUS OF VARIATION ASSIGNMENT
2. DRAWING NOT TO SCALE
3. ALL DIMENSIONS ARE IN MILLIMETERS
4. DIMENSIONS OF EXPOSED PAD ON BOTTOM OF PACKAGE DO NOT INCLUDE

MOLD FLASH. MOLD FLASH, IF PRESENT, SHALL NOT EXCEED 0.15 mm ON ANY SIDE
5. EXPOSED PAD SHALL BE SOLDER PLATED
6. SHADED AREA IS ONLY A REFERENCE FOR PIN 1 LOCATION ON THE

TOP AND BOTTOM OF PACKAGE

## TYPICAL APPLICATION

## CCD Bias Supply



## reLated parts

| PART NUMBER | DESCRIPTION | COMMENTS |
| :---: | :---: | :---: |
| LT1615/LT1615-1 | $300 \mathrm{~mA} / 80 \mathrm{~mA}$ (Isw), High Efficiency Step-Up DC/DC Converters | $\mathrm{V}_{\text {IN }}: 1 \mathrm{~V}$ to 15 V , $\mathrm{V}_{\text {OUT(MAX) }}: 34 \mathrm{~V}, \mathrm{I}_{\mathrm{Q}}: 20 \mu \mathrm{~A}, \mathrm{I}_{\text {sd }}:<1 \mu \mathrm{~A}$, ThinSOT Package |
| LT1944 | Dual Output 350mA (Isw), Constant Off-Time, High Efficiency Step-Up DC/DC Converter | $\mathrm{V}_{\text {IN }}: 1.2 \mathrm{~V}$ to $15 \mathrm{~V}, \mathrm{~V}_{\text {OUT(MAX) }}: 34 \mathrm{~V}, \mathrm{I}_{\mathrm{Q}}: 20 \mu \mathrm{~A}, \mathrm{I}_{\mathrm{SD}}:<1 \mu \mathrm{~A}$, MS Package |
| LT1944-1 | Dual Output $150 \mathrm{~mA}\left(I_{\text {Sw }}\right)$, Constant Off-Time, High Efficiency Step-Up DC/DC Converter | $\mathrm{V}_{\text {IN }}: 1.2 \mathrm{~V}$ to $15 \mathrm{~V}, \mathrm{~V}_{\text {OUT(MAX) }}: 34 \mathrm{~V}, \mathrm{I}_{\mathrm{Q}}: 20 \mu \mathrm{~A}, \mathrm{I}_{\mathrm{SD}}:<1 \mu \mathrm{~A}$, MS Package |
| LT1945 | Dual Output, Pos/Neg, 350mA (Isw), <br> Constant Off-Time, High Efficiency Step-Up DC/DC Converter | $\mathrm{V}_{\text {IN: }}: 1.2 \mathrm{~V}$ to $15 \mathrm{~V}, \mathrm{~V}_{\text {OUT(MAX) }}: \pm 34 \mathrm{~V}, \mathrm{I}_{\mathrm{Q}}: 20 \mu \mathrm{~A}, \mathrm{I}_{\mathrm{SD}}:<1 \mu \mathrm{~A}$, MS Package |
| LT3464 | 85mA (Isw), High Efficiency Step-Up DC/DC Converter with Integrated Schottky and PNP Disconnect | $\mathrm{V}_{\text {IN: }}: 2.3 \mathrm{~V}$ to $10 \mathrm{~V}, \mathrm{~V}_{\text {OUT(MAX) }}: 34 \mathrm{~V}, \mathrm{I}_{\mathrm{Q}}: 25 \mu \mathrm{~A}, \mathrm{I}_{\mathrm{SD}}:<1 \mu \mathrm{~A}$, ThinSOT Package |


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